OF SOUTHWEST PASS ON THE REGIMEN OF VERMILION BAY LOUISIANA

Hydraulic Model Investigation



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PREFACE

The model investigation of the effect of the proposed closure of Southwest Pass on the salinities and hydraulics of Vermilion Bay, Louisiana, was conducted for the Louisiana Department of Public Works, which paid all costs. Authority for the Waterways Experiment Station to perform the work was contained in first indorsement dated 6 August 1954 to a letter dated 29 July 1954 from the Director, Waterways Experiment Station, to the Office, Chief of Engineers, subject "Proposed Model Study of Vermilion Bay, Louisiana."

The investigation was accomplished in the Hydraulics Division of the Waterways Experiment Station during the period December 1955 to December 1956. Waterways Experiment Station personnel who were actively engaged in the testing, analysis, and report phases of this investigation were Mr. Thomas J. Kinzer, Jr., project engineer, assisted by Messrs. A. J. Banchetti and R. V. Puckett. The investigation was conducted under the general supervision of Messrs. E. P. Fortson, Jr., G. B. Fenwick, and H. B. Simmons. This report was prepared by Mr. Kinzer.

During the course of the investigation, monthly progress reports were submitted to the Louisiana Department of Public Works, and numerous conferences were held between WES personnel and representatives of the Department of Public Works. Open house was held at the Waterways Experiment Station on several occasions so that Public Works Department officials and other interested parties could observe the operation of the Vermilion Bay model.

Grateful acknowledgment is made to Mr. E. L. Hendrix of the U. S. Geological Survey who computed the weekly prototype hydrographs used in this study. Special acknowledgment is also made to Mr. Hu B. Myers, chief engineer for the Louisiana Department of Public Works, and Mr. F. N. Hansen, district engineer for the U. S. Geological Survey, for their cooperation and assistance during the model investigation.

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SUMMARY

Use of Vermilion Bay to relieve the shortage of water for rice irrigation in southwest Louisiana has been proposed, but will require some means of reducing salinities in the bay during the irrigation season. Closure of Southwest Pass, which connects Vermilion Bay with the Gulf of Mexico, was proposed as a means of retarding salt-water flow into the bay, and a model study to investigate the proposal was initiated. Before the effectiveness of this plan could be determined for conditions which will obtain in the future, the effect on bay salinities of a reduction in fresh-water inflow as a result of the Old River Control Structure being constructed on the principal fresh-water source, the Atchafalaya River, had to be ascertained.

The model, built to scale ratios of 1:100 vertically and 1:2000 horizontally, reproduced 1860 square miles of the problem area, and included devices for simulating tides, tidal currents, salt-water movement, alongshore currents, fresh-water discharge, and fresh-water withdrawal.

The model tests showed that installation of the proposed closure of Southwest Pass under present conditions of Atchafalaya River discharge would reduce maximum salinities along the west side of Vermilion Bay to a maximum of 1700 ppm for a season of normal runoff and a maximum of 3600 ppm for a season of extremely low runoff. Corresponding maxima for present conditions with Southwest Pass open are in the order of 8000 ppm and 8800 ppm, respectively.

The tests also showed that, in addition to a major reduction in maximum salinities for conditions of both normal and low runoff, closure of Southwest Pass would retard the time of maximum salinity along the west side of Vermilion Bay so that maximum salinity would occur well after the peak of the irrigation season.

The ultimate reduction of the Atchafalaya River flow following completion of the Old River Control Structure will lessen the effectiveness of the Southwest Pass closure in reducing salinities along the west side of Vermilion Bay. Maximum salinity for a season of extremely low runoff, with the control structure in operation, would be of the order of 4400 ppm as compared to 3600 ppm for present conditions of Atchafalaya River flow. The control structure would not decrease the effectiveness of the closure in retarding the time of maximum salinity until after the peak of the irrigation season. Tests of the effect on these salinities of withdrawing 10,000 cfs from the north and west part of the bay demonstrated that the withdrawals would not affect the date of the peak salinity, but would increase the peak salinity by about 2000 ppm; low salinities would be further reduced.

The effect of closure of the pass on recession of a hurricane surge was studied, and though no definite conclusions were obtained, it appears that hurricanes severe enough to affect the salinity of the bay with the pass closed would occur very rarely.

EFFECTS OF PROPOSED CLOSURE OF SOUTHWEST PASS ON THE REGIMEN OF VERMILION BAY, LOUISIANA

Hydraulic Model Investigation

PART I: INTRODUCTION

The Problem

- 1. Although it may seem strange that a portion of the state of Louisiana, through which passes the drainage of a major part of the continent, should have water-supply problems almost as pressing as those of drainage and flood control, such is the nature of the agricultural and industrial demands upon its subsurface and surface waters that southwest Louisiana is experiencing deficiencies in its fresh-water supply. To add to this problem, the region's major streams empty into coastal basins or into the Gulf of Mexico, and when their flows are low because of scanty local rainfall, salt water enters their channels, contaminating both surface water and aquifers.
- 2. Rice irrigation accounts for nearly all the fresh surface-water usage in southwest Louisiana. The Louisiana Department of Public Works reports that the average total flow of surface fresh water into the coastal basins (Vermilion, Mermentau, and Calcasieu) of this region during the irrigation season of April-August, based on a 52-year period of record, is about 725,600 acre-ft, while the current needs are about 1,201,360 acre-ft.
- 3. The Department of Public Works has investigated several plans proposed to remedy this shortage. One of the most promising involves reducing salinities in Vermilion Bay and incorporating the bay into a reservoir system that would also include White, Grand, and Calcasieu Lakes (see plate 1) and would be supplied by the Atchafalaya River through the Intracoastal Waterway. The model study reported herein was concerned primarily with the part of this plan that proposes that Southwest Pass, which connects Vermilion Bay and the Gulf (see plate 2), be closed as a means of retarding salt-water flow into the bay.
 - 4. A major portion of the Atchafalaya River flow consists of water

diverted from the Mississippi River through Old River. Because the amount of water diverted from the Mississippi is reaching proportions detrimental to interests below Old River, the Corps of Engineers is planning to stabilize the over-all amount of this diversion by means of a control structure on Old River. Since stabilization of the Mississippi River flow into the Atchafalaya might affect the salinities in the bay system adjacent to its mouth, this contingency had to be considered in the study of plans for reducing salinities in Vermilion Bay.

Purposes and Scope of the Model Study

- 5. The principal objectives of the model study were: (a) to determine whether the closure of Southwest Pass would reduce salinities in Vermilion Bay to concentrations permissible in irrigation; (b) if so, to determine the effects on the reduced salinities of withdrawing 10,000 cfs for irrigation and industrial use from the north and west parts of the bay; and (c) to obtain data for use, if needed, in evaluating the effects of the Southwest Pass closure on fish and wildlife. After the study was well under way, the question arose of what effect a hurricane tide might have on the improved bay system. Accordingly, determination of this effect was also included in the investigation.
- 6. To obtain the desired information, the Department of Public Works requested the following model tests:
 - a. Hydraulic and salinity verification.
 - b. Long-term salinity verification to 1955 hydrograph.
 - c. Long-term salinity verification to 1954 hydrograph.
 - d. Base test of 1954 published hydrographs repeated for two years.
 - e. Tests of the effects of the Old River Control Structure on Vermilion Bay salinity with the 1954 hydrographs repeated for two years.
 - f. Test of the effects of closure of Southwest Pass on Vermilion Bay salinity using 1954 published hydrographs.
 - g. Tests of the effects of closure of Southwest Pass on Vermilion Bay salinity using 1954 hydrographs with Old River discharge routed through control structure, repeated for two years.

- h. Test of the hydraulic effects of closing Southwest Pass.
- i. Base test of 1955 hydrographs with Old River discharge routed through the control structure.
- j. Test of the effects of closing Southwest Pass on Vermilion Bay salinity during a year of normal precipitation (1955) with the Old River flow routed through the control structure.
- k. Test of the effects on bay salinity of withdrawing 10,000 cfs from the periphery of Vermilion Bay during a year of normal precipitation (1955) with Southwest Pass closed and the Old River discharge routed through the control structure.
- 1. Test of the effects on salinity in Vermilion Bay with Southwest Pass closed of the hurricane surge of 20 September 1947 superimposed upon conditions existing during a year of subnormal precipitation (1954).*

^{*} Hurricane "Audrey," one of the most severe of record, occurred over this area on 27 June 1957, after this study had been completed and the model dismantled.

PART II: THE PROTOTYPE

Location

7. Vermilion Bay is located on the coast of Louisiana, about 30 miles south of Lafayette and about 45 miles west of Morgan City (plate 1). The principal connection between Vermilion Bay and the Gulf of Mexico is Southwest Pass (plate 2), a rather narrow but deep channel about 6 miles in length; however, a second connection with the Gulf lies to the east through West and East Cote Blanche Bays and Atchafalaya Bay. Since conditions in any one of the bays affect (or even control) conditions in the adjacent bays, the entire bay system must be considered as a single unit in any study involving salinity intrusion.

Physical Characteristics

8. The total area of the bay system is about 650 square miles. Depths throughout the system are quite small, the maximum being of the order of 8 to 9 ft. In Southwest Pass the maximum depth is well in excess of 100 ft, but the controlling depth at the Vermilion Bay end is about 8 ft, and that at the gulf end, approximately 10 ft. The entire bay system is separated from the Gulf of Mexico largely by Marsh Island on the west and an extensive shell reef that extends almost unbroken from the east tip of Marsh Island to Point Au Fer. Although the general elevation of Marsh Island is quite low (about 2-3 ft above mgl), the south side of the island is bounded by a coastal ridge, or chenier, that rises to an elevation of about 5 to 6 ft above mgl. The general elevations of the extensive marsh areas that abut on the bay to the west, north, and east are also quite low, being approximately 2-3 ft above mgl for great distances back from the shore line of the bays.

Tides and Tidal Currents

9. The tides in this region of the Gulf of Mexico are of the mixed type, being semidiurnal when the moon is near the equator and diurnal when

the moon is in the tropics. The average semidiurnal range of tide in Atchafalaya Bay at Eugene Island (for location, see plate 3) is about 1.1 ft, and the average diurnal range about 1.9 ft. Since the mean diurnal range is approximately double that of the mean semidiurnal range, while the period of the diurnal tide is about double that of the semidiurnal tide, the velocities of tidal currents throughout the bay system are relatively constant unless affected by wind or other phenomena of a local nature.

Upland Discharge

10. Most of the upland discharge into the bay system is contributed by the main and Wax Lake outlets of the Atchafalaya River. The normal maximum discharge from these sources is of the order of 300,000 cfs, while the normal minimum discharge is about 40,000 cfs. Other tributaries of the system that contribute significant quantities of upland discharge, especially following heavy local rains, include the Vermilion River, Weeks and Petite Anse Bayous, and the Charenton Canal (see plate 2).

Salinity

- ll. The intrusion of salt water from the Gulf of Mexico into the bay system is of the frontal (or well mixed) rather than the wedge type; consequently, there is little difference between surface and bottom salinities at any location. The principal force involved in the vertical mixing of the salt and fresh water appears to be surface wave action, since the velocities of tidal currents throughout the system are too small to produce such complete mixing even though the depths are quite small. Because of the large area and shallow depths throughout the bays, local winds are very effective in producing choppy waves that promote mixing throughout the depth.
- 12. The average salinity of the bay system varies for the most part on a seasonal basis, and is inverse to the Atchafalaya River discharge, reaching a maximum at the time of minimum flow from the Atchafalaya and a minimum at the time of maximum flow. The effects of local runoff from the minor tributaries may reverse the seasonal trend for short periods of time

in certain portions of the bay system, but such effects appear to be insignificant in both extent and duration as compared to the seasonal trend. Salinities throughout the system have been reduced essentially to zero as a result of sustained high discharge from the Atchafalaya River, while maximum salinities of the order of 6 to 8 parts per thousand have been measured along the west and north sides of Vermilion Bay near the end of a period of sustained low Atchafalaya discharge.

13. After a period of high fresh-water discharge that has essentially freshened the entire bay system, the influx of salt water into the system appears to follow a fairly well-defined pattern. The initial intrusion occurs through Southwest Pass into Vermilion Bay; then the saltwater front fans out through Vermilion Bay and into West Cote Blanche Bay. By the time the salt-water front has reached the central portion of East Cote Blanche Bay, the Atchafalaya River discharge has usually decreased to such an extent that the salt water from the Gulf begins to intrude into the western portion of Atchafalaya Bay. Salt water intruding from this source apparently meets that intruding from Southwest Pass in the vicinity of Marone Point. This pattern is capable of considerable variation, however, depending on the local runoff into Vermilion Bay. The evidence that saline intrusion into Vermilion Bay through the Marone Point cross section lags behind that through Southwest Pass was the principal basis for belief that the closure of Southwest Pass would effect a reduction in the salinity of the bay complex.

Alongshore Currents in the Gulf of Mexico

14. Off the coast of Louisiana, the Gulf Stream flows in an easterly direction in the Gulf of Mexico. Since this might create a westerly setting, alongshore current, a salinity range was established about five miles offshore to determine the effect, if any, that this situation has on the distribution of the Atchafalaya discharge. Several salinity surveys were made on this range. These surveys showed that there is a westerly flowing current along the Louisiana shore that moves the Atchafalaya discharge westward, thus affecting the source salinity at the gulf end of Southwest Pass. Although there was no evidence from the offshore surveys that the

current reversed itself or ceased at any time, it was deduced from the model study that either a reversal or a cessation of the westerly current was the only feasible explanation of some of the salinity phenomena observed in Vermilion Bay (prototype).

PART III: THE MODEL

Description

Area reproduced

15. The Vermilion Bay model was a scale reproduction in concrete of approximately 1860 square miles of prototype area. As shown in plate 2, the area reproduced included a portion of the Gulf of Mexico adjacent to the southern coast of Louisiana, Marsh Island, Vermilion Bay, East and West Cote Blanche Bays, Atchafalaya Bay, the mouths of Vermilion River, Petite Anse and Weeks Bayous, the Atchafalaya River from Morgan City to its mouth, and the Intracoastal Waterway from Morgan City to the Vermilion Lock.

Features of model

16. The model included provisions for reproducing prototype tides, tidal currents, salt-water movement, alongshore currents, fresh-water discharges, and fresh-water withdrawals in the modeled area. Fresh-water discharges were measured by Van Leer weirs, and fresh-water withdrawals were measured by means of adjustable V-notch gates. Salt water for filling the gulf portion of the model, and for reproducing the tides therein, was stored in an underground sump equipped for mixing and controlling the concentration of the salt water. Extra roughness was added as needed in the form of metal strips.

Scale ratios

17. The model was constructed to linear scale ratios, model to prototype, of 1:100 vertically and 1:2000 horizontally, with a resulting slope scale of 20:1. Other scale ratios, computed from the linear ratios, were: area, 1:200,000; volume, 1:400,000,000; velocity, 1:10; discharge, 1:2,000,000; and time, 1:200. The salinity scale ratio was 1:1.

Appurtenances

Tidal equipment

18. Tides were simulated by means of a system composed primarily of a header between the model head bay and an underground sump, a discharge line supplying this header, and an automatic, electromechanical valve

between the sump and input point in the header. If the valve was closed, the input was entirely diverted to the model, causing a rapidly "flooding" tide; conversely, if the valve was completely open, not only would all the input return to the sump, but gravity flow from the model as well, causing a rapidly "ebbing" tide. The function of the tide-control machine was to position the valve so as to produce the proper ebb or flood for each instant of the tidal cycle. The apparatus was equipped with a recording device that permitted a visual check of the accuracy of the tide reproduction at all times.

Gages

19. Water-surface elevations were ascertained at hourly intervals during model operation by means of point gages graduated to permit reading to the nearest 0.001 ft in the model, which corresponded to 0.1 ft in the prototype.

Current meter

- 20. Current velocities in Southwest Pass were measured by means of a midget current meter. The meter consisted of five small cups about 0.02 ft in diameter, mounted on a vertical phonograph-needle shaft set in jeweled bearings. One of the five cups was painted white so that the number of revolutions of the meter could be counted visually. Revolutions per second of the meter were transferred to prototype velocity by means of a calibration curve. Calibration of the meter was checked at regular intervals to insure its correct operation.
- 21. Since the shallow depth of the model bays did not permit the complete separation of the two-tenth and eight-tenth depths that would correspond to the depths at which prototype readings were made, the velocity meter was used at middepth and these readings were compared with an average of the two prototype depths. The middepth model velocity was found to be identical with the integrated velocity measured in the prototype by means of a pole float.

Alongshore current

22. In order to reproduce in the model the alongshore current and its freshening effect upon the waters adjacent to Southwest Pass, a pipe was laid along the eastern end of the model gulf for the introduction of salt water, and a pit with a weir at its perimeter was provided at the

western end of the model gulf. The withdrawal of water over the weir drew the fresh water from Atchafalaya Bay westward, and the withdrawn water was replaced by salt water from both the alongshore-current pipe and the ocean head bay.

Prototype Data Requirements

23. Prototype data required for the adjustment and verification of a model to be used for studies involving salinity intrusion throughout the problem area fall into four general classifications: hydraulic data, short-term salinity data, long-term salinity data, and upland discharge data. Such prototype data as were available at the inception of the model study had been obtained sporadically over a wide range of conditions; therefore, it was necessary to formulate and carry out a program for collection of the data needed for the model study. The program was formulated by the Waterways Experiment Station and carried out by the Louisiana Department of Public Works.

Hydraulic data

A total of five tide-recording gages were maintained in the bay system for the duration of the prototype survey. Of these, three (at Cypremort and Salt Points, and Eugene Island) were used for model verification, and are shown in plate 3. The Eugene Island tide gage is maintained by the U. S. Coast and Geodetic Survey (USC&GS), while the other four gages were installed and maintained just for this study by the Louisiana Department of Public Works. Tidal data at these locations were needed for adjustment of the model tide generator to simulate properly tidal phenomena throughout the entire area under investigation. Records of current velocities and directions throughout a complete tidal cycle at the major control sections in the bay system (Southwest Pass, Marone Point, and Cypremort Point) were needed to insure that current velocities and directions in the model would agree with those of the prototype for similar conditions of tide and upland discharge. Current-velocity measurements at the three above-mentioned locations were obtained at hourly intervals for various points in depth. addition to the tide and current data, the upland discharges of all significant tributaries to the bay system were determined as accurately as possible.

Short-term salinity data

25. The short-term salinity data consisted of salinity determinations throughout complete tidal cycles obtained concurrently with and at the same locations, depths, and time intervals used for current-velocity measurements. It was known in advance that the model would not reproduce such prototype salinities in a quantitative manner if the fresh-water discharges at the time of the observations were reproduced on a sustained basis, because prototype data then available indicated that the salinity at a given point in the bay system at a given time was the net resultant of the tide, upland discharge, and local wind conditions that had occurred for an appreciable period prior to the time of the measurements. However, salinity data of this nature were considered essential to demonstrate that the fluctuations (rather than the concentrations) of salinity with tidal phase at given critical locations were the same in the model as in the prototype.

Long-term salinity and upland discharge data

26. Available prototype data at the inception of the model study indicated upland discharge into the bay system to be the controlling factor with respect to the extent and degree of salinity intrusion throughout the bays. Available data also indicated that the response of salinity concentration at any given point to changes in upland discharge was rather slow. This indicated a need for a large number of salinity-sampling stations with a fairly long period between sampling at a given station, rather than a limited number of stations sampled at close intervals. Accordingly, a network of 73 salinity-sampling stations (see plate 3) was laid out over the entire bay system, and sampling operations were carried out at all stations at intervals of from one to two weeks throughout calendar years 1954 and 1955. (The salinity stations were numbered from 1 to 76, but there were no stations corresponding to the numbers 47, 48, and 51.) The upland discharges of the main Atchafalaya River outlet and the Wax Lake Outlet were measured during this entire period, and the discharges of the remaining tributaries to the bay system were computed by the U. S. Geological Survey (USGS). These data comprised the principal basis for the salinity verification of the model described later in this report.

PART IV: VERIFICATION OF THE MODEL

27. Verification of the Vermilion Bay model consisted of: (a) hydraulic adjustment, (b) short-term salinity verification, and (c) long-term salinity verification.

Condition to be Reproduced

28. An equatorial tide was chosen for reproduction in the model, the tidal range at Eugene Island being 0.89 ft. The discharge of the Atchafalaya River measured at Krotz Springs, La. (see plate 1 for location), distributed between the Atchafalaya River and Wax Lake Outlet, was 41,500 cfs, a fairly low flow that resulted in a well-mixed salinity condition in the bays and no salt-water wedge in Southwest Pass.

Hydraulic Adjustment

- 29. Adjustment of the automatic tide control was accomplished through a cut-and-try process of adjusting the amount of up or down movement of the motorized valve for each portion of tidal cycle. The date for which data were reproduced was 17 January 1956.
- 30. After adjustment of the Gulf of Mexico tide had been accomplished, current velocities and tidal heights were observed in the bay portion of the model and found not to conform to prototype data. Additional roughness was added but this was ineffectual because of the low velocities. Flow in Southwest Pass, however, was responsive to changes in roughness.
- 31. Examination of the field data revealed that prototype wind conditions had affected the tidal elevations recorded at Cypremort Point and Southwest Pass. Therefore, only the tidal heights recorded at Eugene Island and Salt Point were used in the model verification. A comparison of these model and prototype tidal heights is shown in plate 4.
- 32. A comparison of the current-velocity measurements obtained in the prototype and in the model-verification tests is presented for surface, middepth, and bottom at Southwest Pass in plate 5, and for middepth

at stations off Cypremort Point and Marone Point in plate 6.

Short-term Salinity Verification

- 33. After hydraulic adjustment of the model was completed, a movable partition was placed in the model just outside the shell reef and across Southwest Pass to separate the simulated Gulf of Mexico and the bay system. The gulf was then filled with water having a salinity of 20,000 ppm, slightly greater than the highest ocean salinity observed in the prototype. The bay system was then filled to high-water level (HW) with fresh water. The tide machine was started and the river and bayou weirs were adjusted, after which the barrier separating the two bodies of water was removed.
- 34. Prototype salinity conditions represent an integration of the forces involved in tidal and fresh-water flows. In the model, where the fresh- and salt-water bodies were separated at the beginning of a test, operation for a considerable period of time was necessary before the forces of the fresh-water and tidal flows could become properly adjusted. Since the observations made in nature represented a transient condition and not a steady state, it was not necessary to run the model to stability. Therefore, salinity determinations were begun after 10 cycles of operation.
- 35. In general, the model bays tended to be more stratified than their prototypes. The addition of roughness did not change this situation because the model currents were not of sufficient velocity to cause mixing. It therefore appeared that some other agency was responsible for the mixing of the salt and fresh water. It was readily apparent that in nature the agency involved was the wind.
- 36. To determine whether wind would be similarly effective in the model, fans of various sizes were set to blow on the water. The fans did prove to be effective, and after many trials, it was found that the best arrangement was a battery of five 14-in. oscillating fans blowing obliquely down upon the water.
- 37. The salinity verification was an attempt to bring the salinity at Southwest Pass, Marone Point, and Cypremort Point into agreement with the observed prototype salinity by reproducing observed discharges. Plates 7, 8, and 9 show the results after approximately 170 tidal cycles. It can

be seen that the difference between surface and bottom maximum salinities at Southwest Pass was about 3000 ppm in the prototype, while in the model they were identical. This is believed due in part to an insufficient knowledge at the time of the effect of alongshore currents. It is probable that in the prototype the surface salinity was reduced by the westward drift of fresh water discharged by the Atchafalaya River.

38. The prototype measurements show both surface and bottom salinities at Marone Point to be higher than those at Cypremort Point. The model salinities at Marone Point were lower than those at Cypremort Point. Examination of the prototype records shows that at no time during the year 1955 were the Marone Point salinities higher than those at Cypremort Point. It was concluded that the prototype verification data represent an unusual condition, the cause of which lay outside the forces being reproduced.

Long-term Salinity Verification

- 39. The real test of the model's adequacy was the ensuing stage of long-term salinity verification in which it was attempted to determine whether the model, reproducing a repetitious tide and the observed or computed hydrographs for all tributaries, could be depended upon to reproduce the changing salinity picture observed in the prototype. The year chosen for this purpose was 1955 because continuous sampling had been done over the entire area for this period. The discharges reproduced in the Atchafalaya River were those measured at Krotz Springs, and since the model did not extend as far upstream as the separation of Wax Lake Outlet from the Atchafalaya River (see plate 2), the total Atchafalaya River discharge was distributed so that 20% passed through Wax Lake Outlet and 80% through the Lower Atchafalaya River. Hydrographs were not available for Vermilion River, Weeks and Petite Anse Bayous, and Charenton Canal; so weekly hydrographs were computed by the USGS. These hydrographs are shown in table 1.
- 40. For this first long-term salinity verification, model operation was begun with the salt water in the Gulf of Mexico and the fresh water in the bay system separated by a long sheet-metal gate extending from Marsh Island to Point Au Fer, and by a block in Southwest Pass. The model was started as of 1 January (prototype), which meant that the first few months,

during which high fresh-water discharges normally occur in the prototype and greatly reduce the bay system salinity, were an adjustment period during which the salinity pattern became established. The prototype low-salinity period occurred about cycle 280, and as the model test emerged from this low, the adjustment was about complete.

- 41. Surface salinities were measured at the stations where prototype measurements had been made. Samples were obtained at the same time of the tidal cycle and on the same date when prototype samples had been taken. Since the tides in the Gulf of Mexico are of the mixed variety, being sometimes diurnal and sometimes semidiurnal, while the model tides were all of the semidiurnal equatorial variety, it was necessary to devise a system to adapt the prototype sampling time to the model. This was done by determining the percentage of the time between high water and the preceding or succeeding low water at which the prototype sample had been taken. The model sample was then obtained at the same percentage of time before or after HW. Comparative model and prototype salinity surveys (year 1955) are shown in plates 10-55 and in table 2. The 1955 salinity verification is shown in plate 56 and in table 2.
- 42. With the model verified to the 1955 salinity condition, it was desired to reproduce the hydrograph of the driest year of record as a base condition with which to compare tests of improvement plans. The least local precipitation in the areas contributory to Vermilion Bay occurred in 1948, with low stages in the Mississippi River and consequently, in the Atchafalaya River. An alternate period was the year 1954, during which the Mississippi and Atchafalaya River stages were at an all-time low, although a few more inches of local precipitation were recorded in 1954 than in 1948. The Department of Public Works was of the opinion that 1954 was the better choice because prototype salinity data were available for 1954, but not for 1948.
- 43. Since salinity data were available for the year 1954, the use of 1954 conditions for the model really amounted to reverification of the model to a new annual condition. The 1954 weekly hydrographs are shown in table 3.
- 44. When reproduction of the 1954 annual salinity data was attempted, it was found that the summer increase in salinity began earlier in the

prototype than in the model, and that the prototype peak salinity not only preceded the model peak but was also higher. An attempt was made to correlate the earlier prototype salinity increase and higher peak for Vermilion Bay with such obvious factors as the mean daily level of the sea, the aggregate tributary hydrographs, and individual tributary hydrographs. No correlation was apparent in any of these cases. Finally, consideration was given to the fact that the salinity increase began at Southwest Pass and progressed to station 3 (see plate 3 for location of salinity stations) and then to station 40. This seemed to indicate that the water in the Gulf of Mexico adjacent to the mouth of the pass had increased in salinity and that the increase had progressed into the bay via Southwest Pass. The only known factor stabilizing gulf salinity at the mouth of the pass at a fairly low figure was the westerly flow of the Atchafalaya discharge along the continental shelf, caused by the backwash of the Gulf Stream. that if by the agency of the wind, or by some other means, the westerly flow of fresh water should be stopped, or its direction reversed, the salinity at the mouth of the pass would suddenly increase. Arrangements were made to reverse the direction of the offshore currents in the model, and the model salinity curves immediately began to follow those of the proto-It was not possible to confirm by means of prototype observations that such current reversals occur in nature, but in the absence of other workable hypotheses, the current reversal was accepted, with reservations, as the cause of the salinity phenomenon observed. The reservations with which this hypothesis was accepted were tempered by the fact that if the current reversal was not the cause of the jump in salinity, its reproduction during tests of improvement plans would make the closure of Southwest Pass less effective, and it would thus act as a safety factor. It was therefore decided to retain the current reversal as a part of the standard testing procedure. The 1954 salinity verification is shown in table 4 and in plate 57.

PART V: BASE TESTS AND TESTS OF IMPROVEMENT PLANS

Salinity Base Test, Existing Conditions

45. After the model salinity verification had been accomplished, a test of existing conditions (base test) was conducted to afford a basis for evaluating the effects of improvement plans. In this test, samples were obtained every second week, and at local HW slack only. Instead of samples being taken at all salinity stations (plate 3), they were obtained only at the following stations in the bay system: 1, 3, 5, 13, 27, 29, 34, 40, 46, and 52. Salinities for this test are shown in plate 58 and in table 5.

Base Test Including Effect of Old River Control Structure

Since it was considered possible that the stabilization of Atchafalaya River discharge resulting from operation of the Old River Control Structure (see paragraph 4) might affect the salinity of the bay system, information concerning the salinities to be expected after the structure is completed, i.e., permanent future conditions, was desired so that improvement plans for Vermilion Bay could be evaluated realistically. order to obtain this information from the model, computations of the flows that would be diverted from the Mississippi River and routed through the control structure according to the performance criteria for the structure were needed. The Office of the President, Mississippi River Commission (the agency in charge of construction and operation of the control structure), was requested to furnish computed flows through the structure under conditions similar to those that had prevailed in 1954, the conditions used in the base test. This was done, and a model test was conducted that was identical with the base test except that the Atchafalaya and Wax Lake hydrographs reflected the effect of the control structure. The duration of the test was two years, the second year being a repetition of the first year's hydrograph. The results of this test are presented in plate 58 and in table 5. Low and high salinity surveys for the two years are shown in plates 59 through 62. The following tabulation compares the maximum

salinity at the indicated stations for published and routed discharges.*

Effect of Old River Control Structure on Peak Salinities for 1954, Southwest Pass Open

	Without Ol Control St		With Old Control St		
Salinity Station (Plate 3)	Date of Peak Salinity	Peak Salinities ppm	Date of Peak Salinity	Peak Salinities ppm	Difference ppm
3 5 13 27 29 34 40 46	Oct 19 Oct 25 Oct 24 Oct 4 Oct 4 Oct 4 Oct 26 Oct 18	10,400 10,800 8,800 8,200 7,400 4,800 9,100 8,800	Oct 10 Nov 27 Oct 24 Sept 30 Oct 4 Sept 26 Oct 16 Oct 16	12,100 11,300 9,800 10,100 10,900 7,600 10,100 10,400	+1,700 +500 +1,000 +1,900 +3,500 +2,800 +1,000 +1,600

Closure of Southwest Pass

Published-discharge condition

47. A dike was placed across Southwest Pass, completely closing it off from the Gulf of Mexico. A salinity test was then conducted that was identical with the base test in all respects except for the closure of the pass. Published hydrographs were used at all weirs. The times of HW slack were changed by the closure of the pass, and a corresponding change was made in the time of sampling. The effects of the closure upon salinity are shown in table 5 and plate 58. High and low salinities are shown in plates 63 and 64. The salinity in Vermilion Bay was reduced by about two-thirds and the period of maximum salinity was retarded by about 85 days so that, with the pass closed, maximum salinity would occur after the rice irrigation season is over. Salinities at stations 27 and 29 in the Marone Point cross section, which represented the source salinity for West Cote

^{*} In this report, "published" discharge refers to historic Atchafalaya River discharges measured and recorded by either USGS or the Corps of Engineers; "routed" discharge refers to flows routed through the Old River Control Structure, as computed by the Office of the President, Mississippi River Commission.

Changes in	Times	of	HW	Slack	at	Major	Sampling	Stations
------------	-------	----	----	-------	----	-------	----------	----------

	_	HW Slack
Ohahi on		Moon over Eugene Island)
Station	with Southwest Pass Open	With Southwest Pass Closed
3	6.0	8.5
5	5.0	7.0
13	6 . 5	7.5
27	6.0	7.5
29	6 . 5	7.5
314	7.0	8.5
40	7.0	7.5
46	7.0	7. 5

Blanche and Vermilion Bays when the pass was closed, remained nearly the same as those of the base test. The typical relation between the base-test and closure-test salinities in West Cote Blanche and Vermilion Bays is shown in the following tabulation:

Effect of Closure of Southwest Pass on Peak 1954
Salinities, Published Discharge

	Date of Pea	: Salinity	Peak Salinity, ppm				
Station	Base Test	Closure	Base Test	Closure	Difference		
3	Oct 19	Jan 9	10,400	3,800	-6,600		
5	Oct 25	Jan 9	10,800	3,800	-7,000		
13	Oct 24	Jan 9	8,800	3,600	-5,200		
3 ¹ 4	Oct 4	Oct 2	4,700	4,500	-200		
40	0ct 26	Dec 11	9,000	3,600	- 5,400		
46	Oct 18	Dec 11	8,800	3,200	-5,600		

Routed-discharge condition

48. A test was next undertaken in which Southwest Pass was closed and the 1954 hydrographs for the Wax Lake Outlet and Atchafalaya River complex were reduced by being routed through the Old River Control Structure. The results of this test are shown in table 5 and plate 58. High and low salinity data are shown in plates 65 through 68. In the following table, salinities are compared at stations 3, 5, 13, 34, 40, and 46 for the published discharge, pass closed, the routed discharge, pass open, and the routed discharge, pass closed, in order to show: (a) the effect of closing the pass against the background of the open pass for the same discharge condition, and (b) the effect of the Old River Control Structure upon salinities in the bays with the pass closed.

Effects o	f Old	River	Cont	trol_	Struct	ture	and	Closure	of
So	uthwes	st Pass	on	1954	Peak	Sali	lniti	.es	

	Date	of Peak Sal	inity .	Peak	Peak Salinity, ppm		
	Published		Routed	Published		Routed	
	Discharge	Base Test	Discharge	Discharge	Base Test	Discharge	
	Pass	Routed	Pass	Pass	Routed	Pass	
Station	Closed	Discharge	Closed	Closed	Discharge	Closed	
3 5 13 34 40 46	Jan 9 Jan 9 Jan 9 Oct 2 Dec 11 Dec 11	Oct 10 Nov 27 Oct 24 Sept 26 Oct 16 Oct 16	Jan 8 Dec 25 Jan 9 Oct 2 Dec 25 Dec 26	3,800 3,800 3,600 4,500 3,600 3,200	12,100 11,300 9,800 7,600 10,100 10,400	4,400 4,500 4,400 4,300 4,800 4,200	

- 49. The tabulation shows that closure of Southwest Pass caused similar shifts in the time of peak salinity in Vermilion Bay for both published and routed discharges. It also shows that salinities in Vermilion Bay were increased by approximately 1000 ppm by the reduction in discharge in Atchafalaya River and Wax Lake Outlet caused by the Old River Control Structure.
- 50. The salinity curves shown in plate 58 indicate that if a lag occurred in the intrusion of saline waters into Vermilion Bay because of the closure of Southwest Pass, a lag also occurred in the recession of the saline waters, so that at the Marone Point cross section (stations 27 and 29), the salinity recession carried over into the succeeding year. This raised the question of whether the slow recession might have a cumulative salinity effect should the second year be extremely dry. Therefore, this test was extended through 1506 cycles, or 780 days. The results of these tests are shown in table 5 and plate 58. There was no evidence at the end of the test that salinity values in Vermilion Bay were increasing because of slow recession.

Effect of closure on the tidal characteristics and hydraulics of Marone Point cross section

51. It was desired to determine the effect of the closure of Southwest Pass on the tidal range and phasing in Vermilion Bay, and the head difference that would exist between the two sides of the closure. Tidal heights for Eugene Island, Salt Point, Cypremort Point, Southwest Pass (bay side), and Southwest Pass (ocean side) are shown in plates 69-70. The tidal range at Eugene Island was decreased by 0.05 ft (0.0005 ft model) by closing the pass, and the plane of tidal fluctuation was raised about 0.1 ft. There was no appreciable difference in the tides at Salt Point. At Cypremort Point the time of high and low water was retarded by about 2 hr. The range of the tide was reduced by 0.3 ft, high water being 0.1 ft lower for the closure than for the base condition, and low water being 0.2 ft higher.

- 52. The tides on opposite sides of the closure structure were 90 deg out of phase, low water in the Gulf of Mexico corresponding to high water in the bay, and high water in the Gulf of Mexico corresponding to low water in the bay. This would produce the greatest possible slope from one side of the structure to the other. For the equatorial mean tide reproduced in the model, a high water of 1.4 ft in Vermilion Bay corresponded to a low water of 0.7 ft in the Gulf of Mexico, producing a head of 0.7 ft. Should the closure be provided with a bypass canal, the slope through the canal would thus be great both at high water and at low water. A gulf high water of 1.6 ft corresponded to a bay low water of 0.82 ft, giving a head of 0.78 ft. At the inner end of Southwest Pass the phasing of the tide was retarded 3.0 hr by the closure.
- 53. The reduction in tidal range inside the bays was not entirely due to the loss of Southwest Pass as a source of tidal flow. The changed phasing of the tide in West Cote Blanche and Vermilion Bays effected a reduction in current velocities in the Marone Point cross section (plates 71-72). It therefore appears that there is little likelihood of scour around the east end of Marsh Island.

Effect of closure on salinity during a normal year

54. As stated earlier, the effectiveness of the closure of Southwest Pass in reducing the salinity of Vermilion Bay was studied first for the year 1954, a low-discharge year approximating the worst conditions of record with respect to water supply. When the plan proved effective under the worst conditions, the Department of Public Works desired to know what salinities to expect for a normal year. Since 1955 was considered a normal year in regard to precipitation, and since the model had already been

adjusted to that year, it was decided to test the effectiveness of the closure of Southwest Pass for the 1955 discharge condition.

- 55. 1955 salinity base test. Although the model had been adjusted to reproduce the 1955 condition, model samples had been obtained on the date and at the time of the prototype samples. A test of one-year duration was therefore undertaken, during which model samples were obtained at high-water slack. In this test, the discharge for the Atchafalaya River-Wax Lake complex reflected the effects of the Old River Control Structure. Salinities for this test are presented in table 7 and plate 73. Low and high salinity data are shown in plates 74 and 75.
- 56. 1955 closure test. Southwest Pass was then closed, and a test of one-year duration was conducted using routed discharge as in the base test. The results of the test are presented in table 7 and plate 73. Low and high salinities are shown in plates 76 and 77. The table below shows the effect of the closure of Southwest Pass for a normal year:

							Peak S	alinity	, ppm
	Dates	and C	ycles of	Peak	Salinit	ies	1954	1955	1955
	1954		1955		1955		Pass	Pass	Pass
Station	Pass Cl	osed.	Pass 0	pen	Pass Cl	osed	Closed	0pen	Closed
3 5 13 34 40 46	Jan 9 Jan 9 Jan 9 Oct 2 Dec 11 Dec 11	722 722 722 722 533 668 668	Nov 13 Nov 19 Nov 13 Nov 6 Nov 7 Nov 12	614 627 614 600 601 612	Feb 3 Feb 6 Feb 6 Oct 30 Nov 27 Jan 9	772 777 777 587 641 723	3,800 3,800 3,600 4,500 3,600 3,200	9,800 9,000 7,500 3,800 7,900 8,000	2,000 2,000 1,700 3,900 2,500 1,200

It can be seen that with Southwest Pass closed, salinity in Vermilion Bay for a normal year is about 2000 ppm less than for the 1954 low-discharge year. While the peak salinity occurred later in the year with the pass closed, no direct comparison of the two years is possible, because the shape of the discharge hydrographs for the two years was not similar. It was assumed in the model study that completion of Southwest Pass closure would be accomplished at low salinity, and it should be noted that low salinity in 1954 was about cycle 35, whereas in 1955 it was about cycle 290.

Effect of Water Withdrawals on Salinity

57. Because of anticipated future surface-water requirements in

southwest Louisiana, it was desired to determine the effect on Vermilion Bay salinity of the withdrawal of 4000 cfs west of Vermilion Lock, and 2000 cfs from each of the following streams: Vermilion River, Bayou Petite Anse, and Charenton Canal. A test of these withdrawals was made for conditions of the 1955 hydrographs routed through Old River Control Structure with Southwest Pass closed. The duration of the test was 803 cycles, or about 416 days. The results of the test are presented in table 7 and plate 73. High and low salinities are shown in plates 78-79. The closure of Southwest Pass was made on cycle 290, and withdrawal of water was begun immediately upon completion of the closure.

- 58. It was found that the date of peak salinity was not appreciably altered by the withdrawals. The salinity of the peak was increased by about 1800 ppm in Vermilion Bay, but the extremely low salinity peak that had characterized the mouth of Vermilion River for the normal runoff year was increased from approximately 1200 ppm to 3600 ppm by the withdrawals. The salinity at station 34 at the mouth of Charenton Canal, which had not been appreciably improved by the closure of Southwest Pass, was not appreciably worsened by the withdrawals, the peak salinity increasing from about 3900 ppm to about 4200 ppm.
- 59. Another pertinent aspect of the effects of the withdrawals was the reduction in the minimum salinity occurring subsequent to the closure of Southwest Pass. Undoubtedly, the cause of this reduction was the fact that the water withdrawn was replaced by fresher water from East Cote Blanche and Atchafalaya Bays. If such withdrawals were continued on a year-round basis, the question might well arise of whether the water of East Cote Blanche and Atchafalaya Bays would be sufficiently fresh at the end of winter to allow this situation to recur year after year. It is believed that the answer to this question lies in the fact that the vast discharges from the Atchafalaya River and Wax Lake Outlet would continue to freshen Atchafalaya and East Cote Blanche Bays during the winter regardless of the withdrawal of 10,000 cfs in the bay complex to the west. If this be the case, the withdrawals tested would continue to be beneficial to the salinity in Vermilion Bay during the rice irrigation season.
- 60. Another aspect of the situation that could not be evaluated in the model was that although the withdrawals would not adversely affect the

salinity of Vermilion Bay during the rice irrigation season, the increase in Vermilion Bay salinity that occurs late in the year would tend to make the salinity of the water withdrawn fairly high. Since this office does not know what salinity can be tolerated in the water withdrawn, the effect of this situation is not evaluated in this report.

Effect of Hurricane on Vermilion Bay Salinity

- 61. The fact that salinity recession from Vermilion Bay becomes very slow when Southwest Pass is closed raised the question of how long a period of time would be required for the dissipation of the effects of a hurricane tide on Vermilion Bay salinity. Accordingly, the hurricane tide of September 1947 was reproduced in the model. This hurricane tide was superimposed upon the astronomical tide at a time corresponding to 1 July of the 1954 runoff year. In addition, the hydrographs of all tributaries to the modeled embayments were altered to reflect the runoff caused by the hurricane precipitation (table 8).
- 62. As stated in paragraph 8, a chenier, or dune, having a crest elevation of about 5 ft above mgl, traverses almost the entire length of the seaward side of Marsh Island. In the model, this dune acted as a barrier and prevented the hurricane surge from crossing the island. The hurricane surge was not of sufficient duration to cause the penetration of salt water through the Marone Point cross section in appreciable quantities, as can be seen in plate 80. Since there were no detectable salinity effects in Vermilion or West Cote Blanche Bays, the test was discontinued.
- 63. After this study was completed, Hurricane Audrey occurred (27 June 1957). While it is not known what effect this hurricane had upon salinity in Vermilion Bay, the elevation of high water at Eugene Island was 7.9 ft mlw. No doubt such a surge would have crossed Marsh Island, and would have introduced a considerable volume of sea water through the Marone Point section and through Southwest Pass by translation. The hurricane conditions simulated in the model study were not severe enough to indicate the results of such a situation.

PART VI: DISCUSSION OF RESULTS AND CONCLUSIONS

Results

Effect of closing Southwest Pass on peak salinities

- 64. For the low-discharge year tested (1954), the closure of Southwest Pass caused an average reduction of 5000 ppm in peak salinity in Vermilion and West Cote Blanche Bays for the published-discharge condition. For the routed-discharge condition, comparison of the base test with the closure test showed that the closure of Southwest Pass caused an average reduction in salinity of 5800 ppm in Vermilion and West Cote Blanche Bays. Comparison of the peak salinities that actually occurred (base test with published discharge) with those of the closure test and routed discharge, which is really a comparison of a dry year under the existing conditions with a dry year after construction of the Old River Control Structure and closure of Southwest Pass, shows that the average decrease in peak salinity will be about 4300 ppm.
- 65. The year 1955, although fairly normal as regards precipitation, began with high salinities, having followed the high-salinity year 1954. For the normal year, the closure of Southwest Pass was compared only with a base condition that reflected the effects of the Old River Control Structure. Closure of the pass for this condition reduced the average peak salinities 5450 ppm below those of the base test. With Southwest Pass closed the peak salinities occurred in February of the following year. Southwest Pass was closed at the period of low salinity, and because of the relatively high discharge from Atchafalaya River and Wax Lake Outlet, which reduced salinities at stations 27 and 29 almost to zero, the salinity in Vermilion Bay continued to diminish until early September when the rice growing season was over.
- 66. Probably the most important effect of closing Southwest Pass, regardless of the discharge condition, was the shift in the phasing of high and low salinity with respect to the discharge hydrographs, or to the seasons of the year. The rice irrigation season in southwest Louisiana is reported to be from April through August. For the 1954 discharge condition with Southwest Pass open and routed discharge, the peak salinity in all

parts of Vermilion Bay came in October, and since low salinity in most of the bay came in June, the period June-August was one of increasing salinities. With closure of Southwest Pass, the peak salinity in the bay as a whole was shifted to January of the succeeding year, low salinity for this condition occurring in May.

Effects of Old River Control Structure

- 67. Results of the tests in which the discharge hydrographs contained the effects of operation of the Old River Control Structure showed that for the dry year of 1954 the average increase in peak salinities in Vermilion and West Cote Blanche Bays attributable to the decreased discharge from the Atchafalaya River and Wax Lake Outlet was 1750 ppm. The maximum increase in peak salinity was 3500 ppm at station 29; the minimum increase was at station 5, where the primary salinity response to changes in gulf currents occurs.
- 68. Within the interior of the bays, not only did the Old River Control Structure increase the peak salinities, but it also increased the low salinities (during the rice season) by considerable amounts. It is important to note, however, that at stations 27 and 29, both of which indicate the source salinity for Vermilion and West Cote Blanche Bays when Southwest Pass is closed, although the increase in peak salinity was great, there was no increase in low salinity. This fact is probably the key to the success of the closure plan.

Effects of water withdrawals with Southwest Pass closed

69. Apparently, withdrawals of water from streams adjacent to Vermilion Bay increase or decrease the salinity of the bay waters depending on the salinity at the Marone Point cross section. When salinity at stations 27 and 29 is low, as it was in June and July 1955, withdrawal of water from the periphery of Vermilion Bay reduces bay salinity because the withdrawals are replaced by fresher water from East Cote Blanche Bay. Conversely, if salinities at stations 27 and 29 are relatively high, as they were in November and December 1955, the result is a higher peak salinity in Vermilion 3ay. The increased salinity of the bay would tend to cause contamination of aquifers outcropping in the respective basins from which withdrawals are

made. It is therefore recommended that withdrawals during winter months be made contingent upon low salinity at the Marone Point cross section. Hurricane tides

70. The hurricane of 1947 was the worst that had passed inland near the problem area prior to the model study. Its intensity was not great compared to intensities of the worst hurricanes that have occurred in the Gulf of Mexico, such as the 1919 hurricane at Corpus Christi that caused the waters to rise to an elevation 16 ft above the predicted high water, or the 1900 hurricane at Galveston. It is reasonable to suppose that such a hurricane will one day move across the problem area.* When it does, water will be driven across Marsh Island and through the Marone Point opening into West Cote Blanche and Vermilion Bays. It is not considered necessary to design a salinity clearing system for these extremes, however, as only a few such hurricanes have occurred since 1886, and on only one occasion have they recurred at the same point (Galveston, 1900 and 1915). The usual type of gulf hurricane does not cause nearly as great a surge as the rare, very severe storms, and the results of the hurricane surge generated in the model are therefore considered fairly typical.

Conclusions

Effects of Southwest Pass closure

71. The closure of Southwest Pass would effect a considerable reduction in salinities in Vermilion Bay for all conditions of discharge. Reductions for low-discharge and normal-discharge years are given below:

	For a Low-discharge Year	For a Normal-discharge Year
Published discharge	5000 ppm	Not tested
Routed discharge	5800 ppm	5450 ppm

The time of the salinity peak would be shifted so as to occur after the rice irrigation season. Although the recession of saline waters from Vermilion Bay would be retarded by the closure of the pass, there would not be a cumulative effect from year to year.

^{*} Hurricane Audrey, which occurred after these tests had been completed, was such a hurricane.

- 72. The closure of Southwest Pass would also result in a retarded phasing of tides, and a reduction in tidal range inside the bays. The changed phasing of the tide in West Cote Blanche and Vermilion Bays would effect a slight reduction in current velocities in the Marone Point cross section. Therefore, there would be little likelihood of scour around the east end of Marsh Island.
- 73. It was found that the closure (for conditions of a semidiurnal tide) affected the phase of the tide in such a way as to generate the maximum possible head differential on the upstream and downstream sides of the closure both at high and low water.
- 74. If a canal should be provided at or near the closure site, the head across the canal at high water inside the bay would be about 0.7 ft for a tide with a range of approximately 1.0 ft.

Effects of water withdrawals

75. The withdraval of 10,000 cfs from the northern and western parts of Vermilion Bay would not affect the date of peak salinity as shifted by the closure of Southwest Pass. Peak salinities would be increased by about 2000 ppm. Low salinities would be reduced, since they occur at a time when the Marone Point cross section is low in salinity. During the low-salinity period, much more water could probably be withdrawn without damage.

Effects of hurricane tides

76. No valid conclusion can be drawn as to the effect upon salinity of the inundation of the problem area by a hurricane surge, or of the effect of the closure of the pass on the recession of such a surge. However, from the fact that the hurricane reproduced in the model study was one of the worst of record until Hurricane Audrey occurred in 1957, and since this reproduced hurricane did not affect the salinity of the area, it appears that the occurrence of hurricanes that would affect the salinity of Vermilion Bay with Southwest Pass closed would be very rare.

Table 1

Weekly Hydrographs, 1955

Discharge in cfs

Week Ending	Atchafala Morgan City	Wax Lake	Bayou Teche	Weeks Bayou, Cypremort Bayou, and Bayou Carlin	Bayou Petite Anse	Vermilion River
Jan 7	74,000	20,000	460	12	14	470
14	110,000	25,000	850	110	125	875
21	130,000	30,000	6,830	940	1,040	3,940
28	110,000	30,000	1,120	20	25	485
Feb 4	80,000	20,000	365	3	3	460
11	95,000	25,000	29,700	2,510	3,010	14,900
18	100,000	25,000	11,000	60	70	695
25	135,000	35,000	14,000	795	955	4,710
Mar 4	155,000	40,000	4,920	5	3	470
11	195,000	50,000	730	2	2	565
18	200,000	50,000	245	6	2	590
25	220,000	55,000	215	1	1	3 7 5
Apr 1	290,000	70,000	295	16	16	165
8	315,000	80,000	210	2	2	350
15	340,000	85,000	19,600	1,740	1,740	9,820
22	300,000	75,000	9,060	7	7	260
29	235,000	60,000	2,190	2	2	290
May 6	210,000	55,000	105	8	5	-95
13	185,000	45,000	60	4	2	-385
20	145,000	35,000	10,200	2,590	1,580	2,800
27	115,000	30,000	8,550	860	525	880
June 3	135,000	35,000	820	1	2	22
10	125,000	30,000	260	85	450	100
17	115,000	30,000	150	25	130	-80
24	105,000	25,000	-15	8	45	-665
July 1 8 15 22 29	100,000 85,000 80,000 85,000	25,000 20,000 20,000 20,000 20,000	805 125 4,260 3,120 1,480	350 30 1,080 435 165	1,910 55 2,050 830 320	555 -280 4,990 2,280 410
Aug 5	80,000	20,000	4,530	905	655	1,850
12	75,000	18,000	8,790	2,240	1,320	2,980
19	60,000	14,000	360	40	240	14
26	55,000	14,000	-40	40	25	-950

(Continued)

Table 1 (Concluded)

Week Ending	Atchafala Morgan City	Nax Lake	Bayou Teche	Weeks Bayou, Cypremort Bayou, and Bayou Carlin	Bayou Petite Anse	Vermilion River
Sept 2	50,000	13,000	965	285	140	285
9	50,000	12,000	325	30	210	740
16	45,000	11,000	165	25	185	70
23	40,000	10,000	180	4	30	120
30	35,000	9,000	180	6	45	215
Oct 7	55,000	14,000	290	45	42	160
14	55,000	13,000	180	5	4	30
21	80,000	20,000	155	2	2	60
28	60,000	15,000	185	2	2	20
Nov 4	45,000	12,000	175	2	2	40
11	40,000	10,000	265	15	17	110
18	45,000	12,000	270	6	7	110
25	45,000	11,000	1,170	230	250	960
Dec 2	60,000	15,000	3,600	1,010	1,350	4,900
9	70,000	17,000	3,070	380	9 7 5	3,680
16	55,000	14,000	560	3	8	255
23	55,000	14,000	425	2	4	305
31	45,000	11,000	540	1	3	350

Note: Atchafalaya River and Wax Lake discharges based on Krotz Springs measurements. Other discharges estimated by USGS. Minus sign indicates withdrawal.

Table 2

1955 Salinity Verification
Salinity in ppm

Sta	Cycle	8	Cycle 21		Cycle 48		Cycle 73		Cycle 79		Cycle 91		Cycle 104		Cycle 114		Cycle 118		Cycle 129		Cycle 143	
No.	Prototype 8630	Model 745	Prototype	Model 1490	Prototype 7110	Model 3380	Prototype	Model 3667	Prototype 3650	Model 3151	Prototype 4560	Model 2693	Prototype 2920	Model 2521	Prototype 3570	Model 2292	Prototype	Model	Prototype 3440	Model 2120	Prototype 1480	
3 29 40	5450	229	6910 9220	917	3540	1260 2349	2500 5670	917 2635	1920 5870	1031	3690 3790	917 1948	2850 3120	687 3094	3620	687 1547	1980 3620		662 2400	573	88 2020	1833 401 859
54	8230	229	9220	1203	7300						742	687	2120	745	3020	401	3020			1318 286	25	229
	Cycle l	L58	Cycle 172		Cycle 184		Cycle 214		Cycle 226		Cycle 228		Cycle 240		Cycle 251		Cycle 267		Cycle 280		Cycle 292	
1 2	2200 2350	1203 1547	2200 2210	917 2000	2080 2120	1031 1260	1170 1380	401 1031	1280	401	1320	802	1140 1130	573 802	1290 1050	458 859	1230	229	1120 920	229 630	1130 1010	229 573
3	1380 1920	2234 2177	1410 3340	2292 1948	1400	1719 1604	179	974 1260	910	859	900	1203	1310 455	802 802	510 262	745 745	1130	745 573	64 560	573 917	840 940	917 917
5	4110	2177	4590	1318	1800	1547	1190	974	1770	745			660 640	745	2510	802	3990	687	730 780	687 802	1620 1180	802
7	4810 3890	1604 1891	4310 3670	2062 1661	2600 2750	1031 1089	1070 940	630 859	1900 1690	802 859			620	630 687	3150 2620	630 859	4090 4340	630 630	940	344	2210	917 974
8 9															3520 3540	802 859			1260 1350	1146 1203	2620 3 220	1260 1375
10 11	2180	1661	2120	1547	2150	1432	650	745	1410	630			960	687	4460 1420	859 573	1420	516	1630 1340	1375 458	3640 900	1260 344
12 13	2350 2520	1089 1089	2020 1840	1146 859	2140 1840	859 745	950 438	573 573	1230 452	458 458			860 1020	573 458	1120 1550	573 401	1430 1310	458 286	1320 455	401 401	1020 472	344 344
14 15	2500 1480	1490 1547	2320 2470	1375 1776	2200 2650	1031 1375	1890 1910	630 573	830 1740	573 917			1220 1530	573 573	1540 1590	516 687	1300 1310	516 516	1070 730	401 516	320 545	344 458
16 17	2010 2520	1776 1432	2600 3280	1432 1661	2350 2600	1375 1547	2030 1570	859 630	1230 910	745 8 5 9			1250 670	1031 687	1530 1030	573 630	1180 1830	802 458	920 720	458 401	650 780	573 344
18	2200 2620	1318	3280 3770	1776 1146	3000 2600	1203	870 880	573 458	1740 1930	859 859			620 545	573 344	1030 2970	802 573	2390 4200	516 458	720 960	573 917	790 1270	516
19 20	2130	859	3470	745	558 545	516	280	229	1210	687			528	229 286	2410	286	1810	4ó1	650	229	435 620	859 344 286
21 22	1170 1160	859 630	1720 1450	745 516	545 592 410	401 458	308	559 559	295 298	286 286	290	229	171 260	172	382 126	229 172	278 178	559 559	197 200	229 172	580	229
23 24	1080 1070	859 802	850 615	458 687	472	458 573	320 405	286			72 285	286 286	148 138	229 229	118 121	172 115			49 7 7	286 229	360 28 8	115 172
25 26	715 542	573 458	595 608	458 344	398 405	401 286	235	229			165 147	344 229	117 111	229 172	118 128	172 172			102 125	229 172	171 104	172 115
27 28	173 40	344 344	149 116	286 286	114	286 286	61	115			29 110	229 229	65 60	172 115	58 48	172 172			37 35 38 45	458 344	162 44	172 172
29 30	86 405	401 458	46 230	286 286	34 32 38	344 172	75 111	229 172			63 65 36 28	286 172	78 45	172 115	45 46	172 115		286	38 45	229 115	56	115
31	308	344 458	330 275	344 344	205	229 401	19 19	172 229			36 28	229 172	77 37	115 115	61	115 115			84 61	115 229	52 72 36	115
32 33 34	415 552	229	205	401	330 452 69	344 344	14 13	172 229			31 25	172	37 36	229 172	50 68 112	172 229			79 30	115 172	53 54	115
34 35	252 290	229 401	61 980	344 286	540	344	97	229	158	229	2)	زنند	112	172	45	172			120	172	89	115 115
35 36 37 38	1500 800	1318 1719	950 2240	1089 1375	1030 1320	458 1318	470 285	229 573	137 690	286 573			147 900	172 573	154 437	172 573	402	516	95 7 0 77	172 344	70 452	115 344 286
38 39	1660 1540	1661 1719	2200 1880	1260 1490	1020 632	1031 1375	225 185	573 573	465 175	458 516			272 125	573 630	140 126	630 516	117 78	344 516	77 87	344 286	810 1010	344 401
39 40 41	1590 1310	1375 974	1530 1500	11 ¹ 46 802	390 241	974 859	70 88	516 401	200 157	573 286	74	458	62 83	516 229	109 112	516 229	96 122	516 516	74	286	1030 960	286 344
42	1760 2080	1604 1318	2260 2170	1318 1375	1660 1690	1318 1203	800 860	573 745	1180 1120	630 573		•	990 1300	458 687	183 1170	458 573	590 920	688 401	50 760	344 401	660 620	344 344
43 44	2330	1776	2220	1719 1661	1710 1940	1719 1375	1400 1280	917 630		713	1320 1280	573 573	1120	458 630	1100	630 573)0		930	229 344	990 1070	344 344
45 46	2475 2200	2005 1260	2170 2320	859	2260	1146	1870	516	1290	229		713	1580 1100	516	730 108	516	1250	344	1150	401	392 66	344
49 50	1930 1550		2050 1970		1960 2040		920 515				970 910		1040		53	172 172			40 33	286 286	66 72	115 115

(Continued)

Sta	Cycle 1		Cycle 1 Prototype		Cycle :		Cycle 2	14 Model	Cycle 2 Prototype		Cycle Prototype		Cycle Prototype		Cycle 2	251 Model	Cycle :		Cycle 2	280 Model	Cycle 2	292 Model
No. 52 53 54	Prototype	Model	Prototype	172		115		115	riototype	115	riococype	Model		115	28 28 28 32 38	115 172 115 115		172	30 36 32 35	229 115 115 344	48 37 36 46	172 115 115 115
55	Cycle (300	Cycle 3	30	Cycle	346	Cycle 3	865	Cycle 1	447	Cycle	466	Cycle	487	Cycle !		Cycle	528	Cycle :	3	Cycle 5	
1	890	286	1220	458	1910	401	2340	458	980	688	2220	802	2800	1203	2920	1719	2700	2463	3050	3266	5530	3838
2 3	890	630	1510 1890	573 1432	1930 1960	687 1661	2020	1146	1240 1910	1203 2578	3050 2850	1375 3094	3990 3840	229 2 3266	3220 3440	2693 3781	3120 3070	3437 4927	3340 3520	4297 4984	8430 5670	5213 5729
4 5	1,600 2,700	1719 2292	3490 4410	2292 2177	1880 6240	2922 2750	1260 1260	4239 3667	2780 4240	2349 3323	3200 6190	4010 3838	4070 5580	4755 2693	3570 3920	5500 4297	3740 3 <u>9</u> 40	5729 5156	4160 5100	5099 5500	5820 6710	5672 5042
6 7	2,800 4,340	1203 1719	4540 4140	1490 2177	5100 5700	1833 2521	1260 1280	2865 4755	4560 3270	2349 3151	6190 6640	3266 2865	6120 7160	3896 4526	3970 4510	4583 4927	3890 39 ¹ 10	4354 6760	4980 5230	5812 5729	7500 7500	4927 5787
8 9	5,200 6,220	1146 2693	4240 5920	3266 3094	7250 7550	3781 3896	1360 1300	5042 4870	5230 5950	3380 3266	6640 7550	5099 5042	6660 7650	4354 5786	4190 4810	52 1 3 5901	4390 5300	6989 6646	5620 7110	6646 5557	7200 8680	5844 595 8
10 11	13,400 690	2865 516	6040 1220	3437 745	8730 2010	4010 1089	1270 2070	5271 1318	8280 1060	3724 1604	8090 2750	5213 2062	8770 2750	6187 2578	6040 2780	6875 2 693	5750 3420	7276 3896	7400 2980	6588 4526	9270 4760	6474 4182
12 13	580 1 ₁ 95	458 458	800 600	458 344	2360 1890	802 458	1890 2300	802 687	790 5 6	1203 1260	2100 2290	1604 1203	30 0 0 2550	2177 2120	2420 2150	2463 2349	2670 2050	3094 2750	2820 2580	4010 3552	4190 4610	3953 3838
14 15	1428 720	573 630	600 1080	458 802	2040 2570	573 1089	2280 2 170	1031 1432	49 662	1203 1432	3440 4560	. 1661 1948	2450 2320	2292 2005	2580 3390	2578 2807	2720 3200	3323 3781	2600	3896	5500	4182
16 17	940 1,960	745 1260	1630 2870	630 1490	2190 5230	1260 2005	1620 1260	1490 2807	1010 2600	1776 1547	5720 6190	1833 3552	2800 3790	2406 2863	3990 3840	3036 4755	3940 3720	3724 5213	4290 4490	4354 3838	6810 7890	4812 4182
18 19	4,540 5,770	1432 1547	3740 3890	1318 2578	6710 4340	2234 2635	1260 1290	3151 3838	3420 3520	1604 2005	5530 6000	4354	4880 5580	3094 5271	3820 3 77 0	4755 6015	3820 3870	4583 5958	4660 4440	4469 4526	7850 6220	4526 4583
20 21	2,670 860	1203 115	3920 1830	573 344	3990 1280	2578 344	1260 890	1661 573	3220 2220	1547 2120	5450 3000	2349 1318	4810 3270	2979 1661	3990 4040	3552 2177	4020 3620	4182 3323	4290 3740	4111 4182	6090 5130	4125 3323
22 23	338 232	115 573	1610 580	286 172	1210 512	172 172	730	286	2090 2260	974 573	2780 2500	802	3080 3390	1833 1375	4310 3370	2865 2177	37 70 3990	2635 3208	3570 3440	3 437 2578	4740 4360	3437 3036
24 25	183 183	172 172	232 215	115 229	548 320	172 172			2400 1940	401 344	2780 3590	630 573	3390 3790	1203 516	4460 3790	1375 974	3970 4210	2521 1833	3640	2292	5100	2292
26 27	415 860	115 115	378 242	172 172	335 385	172 115	530 212	172 286	1820 970	286 344	5600 5650	573	4440 4610	859 1148	3890 3820	1318 2005	4490 4020	2463 2979	3970	3094	5330	1833
28 29	780 480	115 115	152 81	172 286	224 179	172 344	68 58	172 229	1200 1430	229 286	5030 1660	401 401	3740 3000	1089 745	3000 2650	1833 1203	3340 2480	2635 2349	1980	2463	3470	1948
30 31	128 61	115 172	80 84	115 172	132 89	115 115	65 102	344 172	740 362	286 344	1070 970	401 344	1840 1670	745 630	2120 1960	1432 1318	2260 2170	2234 2635	1990	2463	2040	1891
32	56 60	115	87 92	115 115	93	115 172	104 111	115 115	50 99	286 229	1040 800	3 կ.կ	1520 1510	687 630	2100 1800	1089 5 8 9	2490 2400	2005 1776	2010	2349	1460	2062
33 34 35	78 120	286 115	125 155	172 172	97 54 312	172 172	132 150	172 172	71 735	86 286	930 1670	115 344	1130 1550	229 516	1710 2270	286 859	2420 2620	687 1260	1560 2180	1891 2463	13 80 2650	2234 2234
35 36 37	227 850	115 401	506 1870	172 401	750 1930	172 573	295 332	229 573	1840 1820	286 1203	1860 1950	401 1490	2600 3270	688 2177	2380 2950	1669 2463	2900 3050	1490 2979	2980 3420	2406 4125	2900 4410	2521 4526
38 39	700 550	401 401	1680 1720	516 516	1900 1800	630 630	232 228	630 687	1930 1940	1318 1432	2150 2050	1661 1948	3420 3470	1547 2005	2680 2420	2865 3323	3420 3470	3151 3609	3			ŕ
46 41	425 560	401 229	1690 1600	516 516	1640 1540	573 573	480 502	687 573	1970 1960	1089 1203	2030 2180	1719	3440 3250	1089 1891	2680 4040	2635 2578	3520 3720	3725 3437	3300	3896	4490	4182
42 43	478 930	458 401	880 2090	458 401	1440 1820	630 516	1210	859	1940 1710	1031 1146	1940 3050	2005 1089	3150 3920	2578 2349	3000 3540	2979 2807	3970 3370	2979 2406	3340	3609	4340	4640
44	880 940	401 286	1950 1460	516 458	1720 2090	458 573	1990 1760	859 573	1590 1190	974 1146	3050 3300	1432 1203	3720 3370	1604 1719	3270 3200	2463 2521	3320 3370	3609 3667	3370 3120	3953 3896	4740 5620	4411 4411
45 46 49	398 71	458 172	191 85	401 172	1330 95	573 115	1430 52	687 172	182 485	1031	1940 2390	1776 344	840 1880	2005 573	2040 2290	2750 974	1810 2200	2463 1891	1970 2050	4182 2292	5330 2350	4010 2005
50 52	73	229 115	101 70	115	115 36	115 286	84 73	115	258 68	229 229	3520 328	344 229	2140 2920	516 344	2140 1640	859 802	2330 1280	1891 1891	2320 2780	2234	1980 1040	2234 2234
53 54	55 49 302	115	. 73 83	172 172	105 169	286 115	61 58	172 344	220 495	114 458	1980 3340	229 286	3390 3370	401 630	1830 2070	1089 1490	2190 1930	1948	3150 3440	21 7 7 2779	1450 2180	1776 1719
55 56	508	115	156	172	145	286	58	172	1130 43	286 57	4360 73	401 115	3570 1320	802 57	2520 2170	1432 172	2600 1100	2578 172	3620	2750	3420	1776
									_						-							

Table 2 (Continued)

Sta	Cycle 3		Cycle 3		Cycle 346	Cycle		Cycle 1		Cycle 1		Cycle 1		Cycle		Cycle 5		Cycle 5		Cycle (
No.	Prototype	Model	Prototype	Model	Prototype Mode	Prototype	Model	Prototype		Prototype		Prototype		Prototype	Model	Prototype 468	Model	Prototype	Model	Prototype	
57 58								43 47	57 57	101 92	57 115	790 270	57 57	850 82	115 115	115	115 57	1950	1,15	175	172
59 60								47	57	81	86	310	57	94	115	84	57	198	115	180	57
60 61								49 62	86 57	82 212	57 115	1180 740	57 57	740 455	57 86	165 282	57 57	1360	115	135	57
62								51	57	278	57	61	57	590	57 86	145	57				
63 64								47 51	57 57	75 69	57 57	60 57	57 57	168 165	86 57	230 165	57 57	375	57	178	57
65								49	114	82	57	60	57	121	57	84	57	62	57	182	115
66 67								50 50	114 57	83 137	57 57	101 175	57 57	106 172	115 57	2148 282	57 57	94	57	185	57
68								50	114	124	57	57	57	200	57	300	57	920	115	180	57
69 70								56 52	57 57	1280 530	115 57	1730 680	57 57	1010 340	57 57	3570 1202	57 57	2700 1820	229 172	1350 790	57 57
71								130	57	628	57	840	57	278	57	1020	57	2550	57	650	57
72								52 48	57 114	860 1430	115 115	1020 1930	115 57	495 618	57 57	1640 1090	57 57	1770	57	1650	57
73 74								63		2450	57	2550	57	1470	57	1650	57	1660	57	1780	57
75 76								45 46	.57 .57	1190 362	57	2420	57	1500 870	57	1940 2220	57	2650	c m	000	57
70									57	302	57	2350	57	010	57	2220	57	2000	57	990	21
Sta	Cycle 6		Cycle 6		Sta			Cycle 6			Sta No.	Prototype	Model	Cycle 6	Model						
No.	Prototype	Model	Prototype	Model	No.	Prototype	Model 4182	Prototype 3440	Model						2120						
2	5200 4360	4068 5156	4210 3720	1833 4411	20 21		4297	3250	4583 4870		50 52	2310 505	1833 1833	1310 245	573						
3	5600	5672	3120	4640	22		3609	3220	3667		53	1990	2005	2900	1089						
4 5	5430 6760	5500 6245	3370 4740	4698 4755	23 25	4760 4210	3667 2406	2800 2420	2521 2635		54 55	3870 4510	1891 1891	1860 2750	2120 2120						
6	6860	5213	4510	4755	27	4760	2005	2700	2292		57	112	57	115	172						
7 8	7250 7060	5557 5901	4860 4960	4812 4927	29 31	4310 3540	2120 2120	2100 2190	2406 2177		59 61	142 107	172 57	472 260	115 115						
9	7500	6015	5750	5156	32 31		2005	1140	2062		63 65	103	57	65	115						
10 11	7650 4590	5786 4812	6190 3690	5042 4239	31	2880 1120	1948 2062	452 1170	573 2292		65 66	104 102	115 57	64 64	229 115						
12	2750	3953 4469	1820	4125	35 36	1580	2521	2620	1661		68	350	57	68	115						
13	2040 6460	4469 4411	450 575	1719 2979	31 40	3300 4830	4812 4411	4610 3590	4297 4182		69 70	1640 2 8 2	115 57	76 212	115 115						
15 16	5950	4927	575 4540	4812	43	2850	4583	4090	3437		71	462	57	405	115						
17	6410 6760	4755 5042	4830 4830	3838	<u>ц</u> е 46	5820 4460	4411 4526	4260 178	3266 458		72 74	350 155	57 57	178 850	115 115						
18 19	6610	4354	4030 4760	4297 4526	49		1948	1590	2120		76	110	57	920	115						

Table 3

Weekly Hydrographs, 1954

Discharge in cfs

	Atchafala	ya River		Weeks Bayou,	Bayou	
Week	Morgan	Wax	Bayou	Cypremort Bayou, and Bayou Carlin	Petite	Vermilion
Ending	City	Lake	<u>Teche</u>		Anse	River
Jan 8	41,400	10,300	2,160	490	435	1,710
15	41,800	10,500	4,280	1,010	900	3,150
22	51,500	12,900	1,690	100	89	560
29	106,000	26,400	700	7	6	385
Feb 5 12 19 26	155,000 127,000 70,200 64,400	38,600 31,800 17,500 16,000	646 342 310 364	36 0 0	380 0 0 0	475 330 310 340
Mar 5 12 19 26	88,800 84,800 87,200 83,200	22,200 21,200 21,800 20,800	231 226 176 183	0 0 0	0 0 0	320 340 310 250
Apr 2	76,400	19,100	675	63	8	530
9	83,200	20,800	319	14	18	700
16	86,200	21,500	138	1,100	1,470	100
23	95,300	23,800	303	220	295	40
30	105,000	26,200	0.2	235	310	-120
May 7 14 21 28	141,000 174,000 182,000 164,000	35,200 43,400 45,600 41,000	1,050 976 609 120	0 0 0	0 0 0	260 240 -160 -385
June 4 11 18 25	129,000 101,000 100,000 89,600	32,400 25,200 25,000 22,400	-136 -200 -152 -41	0 0 0	0 0 0	-595 -760 -725 -470
July 2	80,000	20,000	-229	0	0	-1,120
9	74,400	18,600	-124	100	44	-630
16	70,900	17,700	-180	6	3	-930
23	58,800	14,700	-155	56	25	-760
30	60,100	15,000	347	3,180	1,410	2,970
Aug 6	58,600	14,700	850	75	120	540
13	41,600	10,400	127	0	66	-790
20	43,800	10,700	-105	0	3	-720
27	43,400	10,800	87	0	2	-190

Table 3 (Concluded)

	Atchafala			Weeks Bayou,	Bayou	
Week	Morgan	Wax	Bayou	Cypremort Bayou, and Bayou Carlin	Petite	Vermilion
Ending	<u>City</u>	Lake	<u>Teche</u>		Anse	River
Sept 3	44,700	11,200	-109	140	46	-770
10	51,100	12,800	101	175	58	-48
17	46,300	11,600	-11	310	100	-505
24	35,900	9,000	87	455	150	-165
Oct 1 8 15 22 29	36,900 41,100 43,900 50,700 67,100	9,200 10,300 4,010 12,700 16,700	102 168 4,010 625 352	39 0 0 0	79 1 390 14 9	-34 100 1,100 405 330
Nov 5	90,300	23,000	630	280	320	415
12	74,700	18,800	257	75	80	190
19	55,900	14,000	227	16	17	96
26	41,900	10,500	198	15	16	81
Dec 3 10 17 24 31	36,900 39,400 46,200 51,200 55,700	9,300 9,900 11,700 13,000 14,600	201 225 360 507 1,460	9 0 0 0	13 0 0 0	40 28 49 95 310

Note: Atchafalaya River and Wax Lake discharges based on Krotz Springs measurements. Other discharges estimated by USGS. Minus sign indicates withdrawal.

Table 4

1954 Salinity Verification
Salinity in ppm

	Sta	3	Sta		Sta 1	3	Sta 2	27	Sta 2	29	Sta 3	1	Sta 3	34	Sta 4	0	Sta 1	16	Sta '	52
Cycle	Prototype	Model	Prototype	Model	Prototype	Model	Prototype	Model	Prototype	Model	Prototype	Model	Prototype	Model	Prototype	Model	Prototype	Model	Prototype	Model
10		1,375										3,094				859		57		
35	2,250	2,005									2,000	1,891			3,750	2,005	125	115		
60		2,750		3,667								1,375				1,661		745		
100		3,437		7,793								974				2,521		1,432		
125		4,411	_	7,390								1,203				3,667		1,375		
143	7,000	7,047	6,250	3,552							3,250	1,260			6 , 500	7,906	1,840	3,036	3,500	516
197	4,000	7,333	4,200	8,537	~						1,500	1,490			3,250	5,672	240	458	1,550	1,203
240			2 222		3,790	1,146									2,110	4,755				
242	3,720	5,901	6 , 660	6,073			1,900	1,375	630	1,547			495	344						
263	1. 01.0	1. 100					1,020	1,146	712	1,260			52	859						
265	4,040	4,182	7 700		2 200											0. (00	400	1,260	340	57
267			7,700	5,099	3,120	2,005									970	2,693		0.065		
305			1,880	2,807	3,720	7,578							248	r1(980	2,979	2,920	2 , 865		
307	2,820	2 026	5,380	4,411			520	573	83	573				516	2,100	2,750				
325 330	2,020	3,03 6	2,770	4.870	3,270	2,406									1 220	2,570	2.000	2,693		
334			4,110	4,010	3,210	•	1,540	286	695	401			186	329	1,330 1,960	2,292	3,200	, , -		
359			11,800	10,714	3,970	4.125	1,540	200		401			100		4,020	4,125	2.070	3,838		
359 361			11,000	10, (14	3,910		3,340	2,693	1,820	1,891			202	229	4,020	4,127	3,070	3,030		
386			12,200	7,448	6,440	7,677	3,340	2,093	1,020	1,091			202		7,270	8,479	5,400	7,677		
386 388		11,000	22,200	1,440	0,440	1,011	6,510	8,652	4,490	8.250			1,350		1,210	0,419	J,400	1,011		
412	8,560	9,796					4,410	6,989	2,600	6,130			270	3,323	8,330	9,109				
414	0,,00	7,190	9,420	6,531	5,430	7,276			2,000	0,130				2,343	0,330	9,109	2,100	6,073		
425			<i>y</i> ,		J, 150		7,010	7,505	3,820	4,583			272	5,271	11,600	7,562				
427					6,540	8,135		1,,,,,,		1,703				J, 2 1 ±		19 202				
429	10,600	10,427	14,900	12,718													5,400	7.104		
460	20,000	10,025	2.,,,00	9,739						5,614		~				8,250	,,	8,479		
493			8,430	10,656	8,920	8,021									6,510	7,906	8,090	6,531		
495	7,500	9,166					5,230	6,588	4,610	5,786			3,050	6,015						
520	7,350	9,854					6,270	7,104	4,140	6.015			3,340	3,838	5,770	7,906				
522			6,370	10,656	7,850	7,104											8,120	7,047		
537	6,490	8,880					7,200	7,734	5,280	6,474			3,270	4,297	5,670	6,302				
541					7,550	7,792											7,890	8,193		
574	7.010	9,568					4,690	6,588	4,640	6,187			3,840	4,297	6,860	8,880				
576			6,710	9,510	6,460	6,588											6,070	6,015		
614			6,020	8,594	5,850	6,474									6,460	8,135	4,830	4,927		
618	6,710	8,937					4,290	5,042	3,250	3,896			460	4,640						
630			7,650	9,854	8,380	8,193									9,600	9, 166	4,090	5,729		
632	9,270	10,885					6,640	4,927	6,410	6,416			1,670	3,437	10,600	9,739				
671			12,600	10,256	9,420	8,193									9,600	8,594	8,970	7,104		
674	9,650	9,568					7,890	5,271	6,710	4,984			880	4,182						
682	9,120	9,739	12,300	8,937	6,710	7,677	8,280	5,786	6,710	4,755			139	2,521	10,200	8,537	6,490	7,505		

Table 5

Salinity Tests, 1954 Hydrographs
Salinity in ppm

		50.11	nicy in							
Condition		3	5	13	27 27	tion 29	34	40	46	52
		Cyc	les 47-48							
Base test, published discharge	400	2,875	2,900	900	2,800	1,825	3,400	1,700	225	570
Base test, routed discharge SW Pass closure, published discharge	573 745	2,807 1,833	1,833 3,437	687 1,604	4,354 2,635	2,979 2,062	2,120 344	3,151 2,406	115 115	2,406 7 45
SW Pass closure, routed discharge	1,490	2,406	2,578	2,349	4,068	3,323	1,089	2,979	286	2 ,7 50
		Cyc	les 74-75	5						
Base test, published discharge	1,575	3,600	4,275	2,100	1,275	1,180	680	2,100	1,400	115
Base test, routed discharge SW Pass closure, published discharge	1,661 1,719	4,010 1,891	3,495 2,693	2,693 1,719	2,693 1,833	1,833 1,146	1,089 401	3,266 2,120	2,234 974	172 172
SW Pass closure, routed discharge	1,719	2,179	2,292	2,292	2,865	2,521	1,146	2,578	1,719	687
		Cycle	es 101-10	02						
Base test, published discharge	2,075	3,600	4,600	2,300	1,025	880	675	2,200	1,675	200
Base test, routed discharge SW Pass closure, published discharge	2,521 2,120	5,271 2,005	4,640 2,635	2,979 1,948	2,635 1,661	2,005 1,375	1,260 516	3,495 2,177	2,292 5 7 3	1,490 630
SW Pass closure, routed discharge	1,891	2,521	2,750	2,292	2 , 349	1,891	1,490	2,865	1,146	1,719
		Cycle	es 128-12	<u>29</u>						
Base test, published discharge	2,670	4,425	6,050	3,000	1,950 3,609	1,600 3,151	800 1,661	3,300	1,800	500
Base test, routed discharge SW Pass closure, published discharge	3,094 1,948	6,015 2,062	3,552 2,922	2,463 2,062	1,432	1,375	802	4,411 2,234	1,318 286	1,719 344
SW Pass closure, routed discharge	2,062	2,693	2,234	2,349	2,635	2,062	1,260	2,521	401	1,948
		Cycle	es 155-15	<u> 56</u>						
Base test, published discharge Base test, routed discharge	4,075 4,068	5,050 6,875	6,125 3,896	4,300 3,838	2,020 3,208	1,950 3,094	1,050 2,120	4,200 4,812	3,725 4,182	860 2 , 292
SW Pass closure, published discharge	2,062	2,062	2,521	2,062	1,375	1,203	745	2,177	1,318	344
SW Pass closure, routed discharge	2,120	2,463	2,292	2 , 349	2,693	2,292	1,260	2 ,40 6	1,661	1,776
		Cycle	es 182 -1 8	33						
Base test, published discharge Base test, routed discharge	4,525 4,525	6,400 7,161	5 ,7 50 6,474	4,650 4,8 7 0	1,900 2,807	1,725 2,863	600 1,260	4,550 4,927	3,825 4,870	1,215 2,120
SW Pass closure, published discharge	2,005	2,120	2,463	2,005	1,203	1,031	516	2,120	1,146	5 7 3
SW Pass closure, routed discharge	2,349	2,578	2,463	2,406	2 ,2 34	2,062	859	2,406	1,318	1,891
			es 209-2		- 0			1		
Base test, published discharge Base test, routed discharge	3,200 6,818	5,600 6,760	4,300 5,614	2,525 1,547	1,850 2,463	1,500 2,406	1,100 1,146	4,100 4,354	3 7 5 1,604	775 917
SW Pass closure, published discharge	1,432	2,120	2,177	1,948	1,318	1,260	é30 859	1,948	458	458 1,891
SW Pass closure, routed discharge	1,203	2,635	2,062	974	1,948	1,833	0)9	2,062	172	1,091
D 4	1 -		es 236-2			. 200	000	a lege	. 750	175
Base test, published discharge Base test, routed discharge	3,240 3,208	4,980 6,302	3,600 5,672	2,400 1,490	1,550 2,349	1,300 2,120	82 0 802	3,475 4,526	750 2,120	175 229
SW Pass closure, published discharge SW Pass closure, routed discharge	1,375	1,891	2,349	1,661 1,260	1,375 1,776	1,260 1,719	286 2 2 9	1,833 1,948	229 172	68 7 28 6
by lass closure, louved discharge	1,661	2,349	2,120	•	۰۱۱۰ و ـ	19 (19	LLJ	2,540	*1-	200
D t	0.700		es 263-20 3,600	2 ,47 5	1,125	1,200	700	2,550	1,100	90
Base test, published discharge Base test, routed discharge	2,700 2,807	3,750 4,354	4,640	2,406	1,547	1,260	344	4,068	2,807	115
SW Pass closure, published discharge SW Pass closure, routed discharge	1,260 1,490	1,490 1,833	2,120 1,776	1,375 1,661	1,031 1,604	1,089 1,604	115 115	1,490 1,776	917 401	115 1 7 2
on rade onesate, remain continues	_, ,,			_	,	·		• • •		
Base test, published discharge	2,700	3,275	es 277 - 2 2 , 925	2 , 525	775	700	600	2 , 575	2,300	115
Base test, routed discharge	3,151	4,698	3,667	3,094	974	917	458	3,266	3,266	115
SW Pass closure, published discharge SW Pass closure, routed discharge	1,375	1,604	2,349	1,490	974	917	229	1,490	1,375	115
,		(tve1	es 290 - 2	91						
Base test, published discharge	2,520	3,050	2 , 575	2 , 875	500	400	600	2,425	3,000	150
Base test, routed discharge	2,865	4,411	3,495	3,208	745	458	458	3,266	3,552 1,490	115 115
SW Pass closure, published discharge SW Pass closure, routed discharge	1,490 1,719	1,490 1,891	1,891 1,776	1,490 1,833	802 1 , 375	630 1 , 089	229 386	1,490 1,719	1,661	172
•		-	04-305-3							
Base test, published discharge	2 , 350	3,100	3,275	2,250	400	350	400	2,000	2,875	125
Base test, routed discharge	3,094	4,469	4,354	3,552	458	286	458 401	2,750	4,870 1,490	115 115
SW Pass closure, published discharge SW Pass closure, routed discharge	1,490	1,490		1,490	802	573		1,547		
•										

Table 5 (Continued)

					St	ation	··			
Condition	1	3	_5	13	27	29	34	40	46	52
		Cycl	es 317-3	18						
Base test, published discharge	2,200	3,100	3,380	2,325	400	425	350	2,125	2,700	200
Base test, routed discharge SW Pass closure, published discharge	2,521	4,411 1,547	4,469	3,380	286	5 7 3	344	3,151	3,953	115
SW Pass closure, routed discharge	1,547	1,776	1,776 1,948	1,432 1,891	573 917	458 7 45	458 458	1,490 1,719	1,546 1,661	172 172
			•	•				-,,-,	_,	-1-
Done to the model of the State			es 330-3							
Base test, published discharge Base test, routed discharge	2,275 2,521	3,500 4,698	3,975 3,838	2,250 3,323	400 401	400 401	300 286	2,250 3,437	2,750 3,953	160
SW Pass closure, published discharge	1,604	1,604	2,521	1,490	630	458	401	1,490	1,490	115 229
SW Pass closure, routed discharge										
		Cycl	es 344-3	45						
Base test, published discharge	2,250	3,700	4,175	2,350	425	300	200	2,580	2,550	115
Base test, routed discharge SW Pass closure, published discharge	2,292 1,490	4,640 1,375	3,781 1,547	2,349 1,432	458 516	286 344	286 5 7 3	3,036 1,490	2,463 1,490	172 172
SW Pass closure, routed discharge	1,719	1,948	2,005	1,719	859	573	859	1,719	1,719	458
	9	Cycles 3	60-361-3	62 - 363						
Base test, published discharge										
Base test, routed discharge SW Pass closure, published discharge										
SW Pass closure, routed discharge	1,719	1,833	1,891	1,719	687	573	802	1,547	1,661	401
		Chrol	on 2771 21	-					•	
Dana danda mulhildahad didanbanan	2,690		es 371-3	_	hor	200	200	0.050	2 200	202
Base test, published discharge Base test, routed discharge	2.865	4,475 5,443	5,025 4,411	2,800 2,979	425 630	300 458	300 401	2,350 3,667	3,300 3,437	220 286
SW Pass closure, published discharge	1,490	1,490	1,490	1,375	458	401	458	1,375	1,490	172
SW Pass closure, routed discharge	1,776	1,833	1,833	1,661	745	573	802	1,719	1,719	401
		Cycle	es 385 - 38	<u> 36</u>						
Base test, published discharge	2,950	4,950	5,650	3,225	550	300	200	2,580	3,400	280
Base test, routed discharge SW Pass closure, published discharge										
SW Pass closure, routed discharge										
		Cycles	398-399	-1400						
Base test, published discharge	2,720	5,750	5,575	3,675	675	300	225	2,425	3,700	425
Base test, routed discharge	3,323	6,416	4,297	4,125	1,432	1,203	286	5,500	3,838	859
SW Pass closure, published discharge SW Pass closure, routed discharge	1,375 1,661	1,547 1,661	1,490 1, 7 19	1,375 1,604	516 974	458 859	1 7 2 401	1,490 1,547	1,318	172 687
on last closure, louded discussing	1,001	•		-	דוכ	0)9	401	±•)+1	1,661	001
Base test, published discharge	2,260	5,350	es 412-4: 5,750	1 <u>3</u> 3,800	1,250	625	200	2,820	3,980	650
Base test, routed discharge								2,020		
SW Pass closure, published discharge										
SW Pass closure, routed discharge										
			426-427		- 0			- (0-	0
Base test, published discharge Base test, routed discharge	3,020 3,151	6,200 6,302	5,300 4,297	2,950 3,896	1,825 2,292	1,350 2,463	275 401	2,625 4,755	4,980 4,984	850 1,719
SW Pass closure, published discharge	1,031	1,776	1,948	1,490	687	687	115	1,375	1,375	688
SW Pass closure, routed discharge	1,432	1,833	1,719	1,604	1,776	1,318	344	1,604	1,661	974
		Cycle	es 439-41	+0						
Base test, published discharge	3,025	5,375	4,950	3,800	2,475	1,600	380	3,125	4,300	750
Base test, routed discharge SW Pass closure, published discharge										
SW Pass closure, routed discharge										
		Cycle	es 452-45	53						
Base test, published discharge	3,490	5,900	6,400	4,450	2,525	2,400	875	3,300	4,600	1,190
Base test, routed discharge	4,469	7,505	6,875	5,094	6,187	5,328	1,490	4,698	5,786	4,182
SW Pass closure, published discharge SW Pass closure, routed discharge	1,318 1,547	1,661 1,719	1,490 1,719	1,375 1,547	1,260 3,552	1,260 3,036	344 974	1,260 1,604	1,432 1,661	516 1,891
dadame, router didentife					ے ری و	J, ~J~	217	_, 00-	-,001	-,054
			63-464-40		_			1 5		_
Base test, published discharge Base test, routed discharge	4,180	6,275	8,050	4,450	3,950	3,100	2,600	4,400	5,200	2,175
SW Pass closure, published discharge										
SW Pass closure, routed discharge										

Table 5 (Continued)

Condition						ation	37.	1.0	106	<u> </u>
Condition		- 3 Creal	<u>5</u> es 479-48	13	27	29	34	40	46	52
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	4,850 5,729 1,490 1,547	6,525 9,625 1,833 1,776	9,425 7,161 1,661 1,948	5,150 6,989 1,490 1,604	4,875 7,276 5,042 6,245	3,600 7,906 3,036 6,187	2,000 4,125 917 2,693	5,000 7,161 1,547 1,891	5,500 6,989 1,490 1,604	2,700 7,219 1,948 5,042
		Cycl	es 506 - 50	<u> </u>						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	6,225 6,932 1,661 1,661	9,100 10,941 1,848 1,776	8,925 9,968 1,833 1,948	6,825 8,594 1,661 1,776	6,000 9,052 6,302 9,052	5,050 9,739 5,271 8,823	2,800 6,875 2,807 5,213	6,000 8,364 2,406 2,922	5,620 9,052 1,604 1,719	3,975 8,937 4,927 7,390
	•		es 520-52							
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	7,025 7,505 1,661	9,400 11,000 2,177	9,825 10,885 1,948	7,550 9,052 1,719	6,680 10,083 7,390	6,375 10,312 6,359	3,650 7,448 3,667	7,275 8,823 2,635	7,050 9,166 1,661	5,600 9,854 5,672
		Cycl	es 533 - 5	34						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	7,450 8,135 1,776 1,776	10,300 11,458 2,349 2,177	8,825 8,364 1,948 2,005	8,325 9,280 1,948 1,948	8,200 10,083 9,052 11,000	7,350 10,885 6,932 10,312	4,775 7,448 4,469 6,351	8,000 9,396 3,094 3,495	8,000 9,739 1,833 1,833	6,500 10,083 5,328 9,854
		Cycl	es 54 7- 51	<u>48</u>						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	7,875 8,651 2,005	10,175 12,131 2,406	9,900 10,198 2,863	8,675 9,625 2,177	7,875 9,911 7,620	7,100 10,771 7,448	3,300 2,177 1,031	8,725 9,682 3,266	8,200 9,968 1,776	7,120 10,251 8,021
		Cycles 5	60-561-50	62 - 563						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	8,190 8,594 1,948 2,120	10,425 11,744 2,750 2,750	9,500 9,510 2,635 2,292	8,800 9,625 2,292 2,349	7,025 9,396 7,276 9,396	6,780 10,255 6,302 9,223	3,700 4,927 3,781 4,870	8,675 10,083 3,437 4,182	8,800 10,312 1,833 1,776	6,675 8,880 6,818 8,823
		Cycl	es 5 74- 5'	<u>75</u>						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	8,500 8,937 2,292	10,100 11,802 2,750	10,800 9,625 2,463	8,775 9,854 2,635	6,475 8,594 6,474	6,000 9,166 4,812	3,900 6,302 3,151	9,125 9,625 3,495	8,050 9,740 2,062	6,200 8,937 5,901
		Cycl	es 58 7- 58	<u>88</u>						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	8,400 8,937 2,635 2,578	9,750 11,229 2,979 3,094	9,825 9,510 2,635 2,635	8,800 9,281 2,922 2,750	6,050 8,250 4,411 7,791	4,900 7,963 3,896 6,875	4,150 5,328 3,437 5,443	8,825 9,052 3,495 4,469	8,325 9,396 2,005 2,062	4,375 5,213 4,469 7,333
		Cycl	es 601 - 6	02						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	8,275 9,109 2,922	9,525 10,943 2,979	9,400 9,109 2,922	8,700 9,223 2,922	5,300 7,505 3,896	3,825 5,958 3,151	2,780 6,588 3,208	8,225 10,083 3,323	7,675 9,682 2,177	3,540 4,812 4,755
		Cycl	es 614 - 6	15						
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	8,240 8,995 2,922 3,380	9,550 11,114 3,437 4,182	8,500 9,510 2,922 3,552	8,200 9,396 3,036 3,437	4,825 7,161 4,870 7,161	3,250 5,156 2,922 4,526	3,200 5,614 3,036 5,443	8,525 9,281 3,380 4,354	7,900 9,682 2,863 2,865	4,025 5,156 4,239 5,729
			es 641-6			_ •				0-
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	8,250 9,052 3,323 3,896	9,400 10,656 3,208 3,781	9,100 11,343 3,323 4,239	8,050 9,281 3,208 4,010	3,700 6,015 3,781 5,844	3,400 5,385 3,208 5,156	3,350 5,443 2,521 3,724	7,725 9,166 3,667 4,583	6,875 9,682 2,922 3,380	3,980 5,385 4,068 5,729
			es 668 - 6					_ ^-		
Base test, published discharge Base test, routed discharge SW Pass closure, published discharge SW Pass closure, routed discharge	7,560 8,765 3,437 4,068	8,775 10,427 3,552 4,297	8,625 9,797 3,437 4,297	7,850 9,567 3,323 4,239	4,175 7,161 4,239 6,359	3,000 6,646 3,781 5,672	2,650 4,927 2,349 2,693	7,800 8,078 3,609 4,526	7,900 9,338 3,208 3,896	3,900 6,187 3,724 4,927

Table 5 (Continued)

expension process with the control of the first of the Control of						ation				
Condition	_1_	3	5	13	27	29	34	40	46	52
Page test muhlished dischange	7 800	9,000	8,800), 200	3,825	1 600	8,200	9 275	2 700
Base test, published discharge Base test, routed discharge	7,800 8,708	10,427	8,995	8,300 9,223	4,200 7,677	7,161	1,600 4,125	9,052	8,375 9,223	3,790 6,818
SW Pass closure, published discharge SW Pass closure, routed discharge	3,552 4,297	3,667 4,297	3,609 4,583	3,552 4,297	4,469 5,500	4,068 5,729	1,3 7 5 2,234	3,667 4,812	3,151 4,239	3,609 5,271
		Cycle	es 722 - 72	23						
Base test, published discharge	4,984	8,308	7,448	5 , 958	3,838		3,266	6,531	4,984	3 ,7 24
Base test, routed discharge SW Pass closure, published discharge	6,187 2,922	10,198 3,838	8,021 3,896	5,729 3,552	6,989 4,297	7,448 4,469	1,432 859	8,594 3,323	4,812 1,490	7,333 3,896
SW Pass closure, routed discharge	3,151	4,411	4,469	4,469	5,614	5,958	1,432	4,297	1,318	5,500
		Cycles 7	+9-750-7	51 -7 52						
Base test, published discharge Base test, routed discharge	5,042 5,786	7,276 9,396	7,219 6,646	5,271 7,948	1,260 6,981	1,260 7,219	3,437 3,323	4,297 7,677	4,984 3,667	1,661 2,979
SW Pass closure, published discharge SW Pass closure, routed discharge	3,151	3,495	3 , 208	3,323	3,724	3,495	1,776	3,437 3,896	2,635 2,578	2,177 4,068
on tube closure, reacon absolute	3,495	4,239	4,010	3,781	5,901	5,328	3,266	3,030	د , ار	+,000
Base test, published discharge	3,208	6,531	∍s 776-7 4,698	<u>11</u> 3 , 724	2,005	630	172	2,521	1,547	630
Base test, routed discharge SW Pass closure, published discharge	5,958	9,339	7,276	8,995	5,099	3,296	3,036	7,677	5,213	917
SW Pass closure, routed discharge	3,094 3,724	3,437 4,239	3,323 4,068	3,323 3,896	3,266 4,354	2,120 3,552	1,661 516	3,437 4,125	2 ,7 50 2 , 865	172 1,375
		Cycle	es 803-80	04						
Base test, published discharge	3,266	5,099	4,927	3,151 8,021	1,146 4,354	1,146	745	3,609 8,307	1,719 4,984	5 7 3 3,437
Base test, routed discharge SW Pass closure, published discharge	7,104 3,036	10,943 3,495	8,307 3,495	3,266	2,292	3,724 1,432	2,349 1,547	3,208	2,062	917
SW Pass closure, routed discharge	3,838	4,297	4,239	3,953	3 ,83 8	2,807	1,432	4,010	1,891	2 , 979
Description with the description of the control of	2 702		ев 830 <u>-8</u> ;	_	3 275	1 202	lion	0 625	Rolo r	458
Base test, published discharge Base test, routed discharge	3,781 6,474	5,099 11,516	6,130 7,161	2,979 8,078	1,375 4,927	1,203 4,297	401 2,177	2,635 9,052	1,948 3,208	3,036
SW Pass closure, published discharge SW Pass closure, routed discharge	2,865 3,552	3,208 4,125	3,208 4,125	3,094 3,896	2,349 3,380	1,948 2, 7 50	1,260 1,661	3,266 3,838	974 1,260	1,490 2,463
		Cycle	es 846-81							
Base test, published discharge										
Base test, routed discharge SW Pass closure, published discharge	2,750	2,979	3,094	2,807	2,349	1,891	1,049	3,151	2,062	1,547
SW Pass closure, routed discharge										
		Cycl	es 857 - 8	<u>58</u>						
Base test, published discharge Base test, routed discharge	3,455 7,791	4,927 10,771	6,531 8,135	3,437 8,594	2,463 4,870	1,776 4,010	745 2,693	4,239 6,989	3,781 7,333	172 3,266
SW Pass closure, published discharge SW Pass closure, routed discharge	3,838	3,781	3,896	3,667	2,979	2,062	1,490	3,380	2,865	1,375
5, 1000 02002 , 100002 0220202g0	3,030			-	4,717	2,002	1, 490	J, J00	2,007	-9317
Base test, published discharge	4,755	6,302	es <u>884-8</u> 7,104	9 <u>2</u> 4,640	1,547	1,432	687	5,156	4,411	573
Base test, routed discharge SW Pass closure, published discharge	7,791	10,141	6,703	7,963	4,182	3,781	2,406	6,302	7,219	3,667
SW Pass closure, routed discharge	3,552	3,667	3,838	3,609	2,463	1,833	1,318	3,724	2,807	1,891
		Cycl	ев 911 - 9	12						
Base test, published discharge Base test, routed discharge	3,781 5,099	5,786 8,708	5,729 4,984	4,010 5,786	1,432 3,896	1,260 3,208	516 1,54 7	4,755 6,359	2,234 1,146	687 2,463
SW Pass closure, published discharge										
SW Pass closure, routed discharge	1,948	3,208	3,208	3,036	2,807	2,292	1,089	3,266	172	2,062
Page test muhlished discharge	3,896	Cycl 4,812	es 9 <u>38-9</u> 6,073	<u>39</u> 3,266	1,203	1,089	229	4,010	1,375	172
Base test, published discharge Base test, routed discharge	4,354	7,333	2,979	4,010	3,208	2,635	1,031	4,068	1,490	286
SW Pass closure, published discharge SW Pass closure, routed discharge	2,292	3,495	2,578	2,750	2,349	2,177	573	2,750	172.	687
		Cycl	es 965 - 9	66						
Base test, published discharge	2,865	2,750	4,010	2,292	745	745	745	2,177	1,719	57
Base test, routed discharge SW Pass closure, published discharge	3,495	5,844	3,323	3,552	1,776	1,089	458	2,693	2,578	172
SW Pass closure, routed discharge	2,062	2,234	2,234	2,292	2,005	1,948	344	2 , 5 7 8	1,490	115

Table 5 (Continued)

			. 		St	ation				
Condition	<u> </u>	3	5	13	27	29	34	40	46	52
Page hash multidated 24 advances	0		es 979-9		-11		1-0	. 0	- 1-6	
Base test, published discharge Base test, routed discharge	2,578 3,437	2,005 4,927	3,380 3,896	1,948 3,896	344 1,031	516 516	458 573	1,833 2,807	2,406 4,068	57 115
SW Pass closure, published discharge SW Pass closure, routed discharge										
		(Terra)	~~ 000 0	02						
Base test, published discharge	2,406	2,635	es 992-9 2,521	<u>93</u> 1,776	401	401	344	745	2,292	57
Base test, routed discharge	3,380	4,411	2,750	3,437	458	229	458	2,979	3,552	115
SW Pass closure, published discharge SW Pass closure, routed discharge	2,406	2,635	2,578	2,463	1,719	1,375	630	2,406	2,292	172
	Cv	cles 100	6-1007-1	008-1009	•	•		•	-	
Base test, published discharge	2,120	2,292	2,349	1,604	344	344	344	917	1,948	172
Base test, routed discharge SW Pass closure, published discharge	3,208	5,099	4,927	2 , 865	458	401	5 7 6	2,693	4,010	115
SW Pass closure, routed discharge										
		Cycle	s 1019-1	020						
Base test, published discharge Base test, routed discharge	2,292	2,120	2,578	1,719	286	286	458	1,031	2,292	115
SW Pass closure, published discharge	3,151	4,239	3,495	2,635	573	344	401	3,266	4,010	172
SW Pass closure, routed discharge	2,578	2,292	2 , 635	2 , 349	1,203	859	401	2 ,40 6	2,463	286
		Cycle	s 1032-1	033						
Base test, published discharge Base test, routed discharge	1,146 2,693	2,578 4,297	3,495 2,234	1,604 2,807	286 516	286 344	286 286	1,719 2,463	2,005 3,323	172 172
SW Pass closure, published discharge										
SW Pass closure, routed discharge										
			s 1046-1			- ((1-0			1-0
Base test, published discharge Base test, routed discharge	2,062 2,865	2,922 5,213	3,437 5,557	2,062 3,208	366 573	366 286	458 286	2,062 3,437	2,177 3,266	458 229
SW Pass closure, published discharge SW Pass closure, routed discharge	2,463	2,292	2,578	2,406	859	630	573	2,406	2,406	458
on rubb crosure, roused arrowings	-,.05	•	•		977	0,0	713	2,100	2,100	1,00
Base test, published discharge	2,635	4,182	s 1073-1 5,271	2,635	366	366	286	2,865	2,578	172
Base test, routed discharge	3,667	6,531	7,161	3,552	802	516	286	4,526	4,354	401
SW Pass closure, published discharge SW Pass closure, routed discharge	2,292	2,120	2,578	2,292	859	573	630	2,062	2,292	573
		Cycle	s 1100-1	101						
Base test, published discharge	2,807	5,672	7,047	3,323	516	401	172	3,094	2,979	229
Base test, routed discharge SW Pass closure, published discharge	3,151	7,619	7,791	4,927	1,661	1,260	286	5,901	4,927	802
SW Pass closure, routed discharge	1,719	2,177	2,406	2,177	1,031	802	286	1,490	2,177	630
	Су	cles 110	8-1109-1	110-1111						
Base test, published discharge										
Base test, routed discharge SW Pass closure, published discharge										
SW Pass closure, routed discharge	630	2,177	2 , 635	2,120	1,661	1,146	286	1,146	1,833	802
			s 112 7- 1			_				
Base test, published discharge Base test, routed discharge	2,750 3,268	4,984 8,300	6,646 8,500	2,750 5,850	1,031 2,292	802 2,463	115 1,031	2,005 4,755	3,036 4,984	344 1,719
SW Pass closure, published discharge SW Pass closure, routed discharge	1,776	1,948	2,349	2,120	1,719	1,375	458	1,432	2,120	974
Dir Tass Closure, Touted discussing	1 ,110			•	+ 91+2	±) 317	,,,,	ے ر ۲۰ وید	2,120	217
Base test, published discharge	2,807	5,156	в 1154-1 4,640	3,380	2,005	1,891	917	3,323	3,495	630
Base test, routed discharge	4,469	8,950	9,150	6,750	6,187	5,328	2,234	4,698	5 , 786	4,182
SW Pass closure, published discharge SW Pass closure, routed discharge	1,948	2,234	2,062	1,833	3,323	2,349	1,089	1,833	2,234	1,033
		•	s 1181-1	_						
Base test, published discharge	3,896	5,672	6,989	4,125	3,437	2,578	1,260	3,896	4,297	1,031
Base test, routed discharge SW Pass closure, published discharge	5,729	9,625	9,800	7,700	7,276	7,906	4,125	7,161	6,989	7,219
SW Pass closure, routed discharge	1,833	2,120	2,062	1,948	4,870	4,068	1,375	2,292	1,948	3,323

Table 5 (Continued)

						ation				
Condition		3	5	13	27	29	34	40	46	52
Dans took such land a descharing	1. 1.33		s 1208-1		h 205	2 020	7. (a):	2 200	l. com	0.1.60
Base test, published discharge Base test, routed discharge	4,411 6,932	6,818 10,541	6,187 10,500	4,182 8,600	4,125 9,052	3,208 9,739	1,604 6,875	3,208 8,364	4,92 7 9,052	2,463 8,937
SW Pass closure, published discharge SW Pass closure, routed discharge	1,891	2,521	2,177	2,062	8,021	6,187	2,578	2,463	2,120	6,073
•	, -		s 1222-1	•	•	, ,	,,,	,	•	, ,,
Base test, published discharge	5,099	8,652	9,396	6,073	4,698	3,896	1,948	4,640	6,245	3,266
Base test, routed discharge	7,505	11,000	10,885	9,050	10,083	10,312	7,448	8,823	9,166	9,854
SW Pass closure, published discharge SW Pass closure, routed discharge								~		
		Cycle	1235-12	36						
Base test, published discharge	5,213	8,364	9,510	5,844	6,302	4,469	2,062	6,073	5,786	4,125
Base test, routed discharge SW Pass closure, published discharge	8,135		8,364	9,280	10,771	10,885	7,448	9,396	9,739	10,083
SW Pass closure, routed discharge	1,948	2,635	2,349	2,177	6,416	5,213	2,693	2,922	2,234	3,724
			s 1249-1					_		
Base test, published discharge Base test, routed discharge	6,416 8,651	8,651 12,031	10,369 10,198	6,130 9,625	6,187 10,198	5,500 10,771	1,719 2,234	7,276 9,682	6,531 9,968	4,698 10,251
SW Pass closure, published discharge SW Pass closure, routed discharge										
bw rass closure, routed discharge										
			2-1263-1		• .	E 7700	0 625	7 222	7 701	4,698
Base test, published discharge Base test, routed discharge	7,104 8,594	9,739 11,774	8,937 9,510	7,161 9,625	6,302 10,427	5,729 10,255	2,635 5,385	7,333 10,083	7,104 10,312	8,880
SW Pass closure, published discharge SW Pass closure, routed discharge	2,177	2,578	2,578	2,521	5,328	4,870	1,719	2,922	2,062	4,755
	,		s 1276-11		,,-	,	,	•		,
Base test, published discharge	7,310	8,995	9,223	6,989	5,271	5,156	3,609	7,505	6,818	5,156
Base test, routed discharge	8,937	11,802	9,625	9,854	8,937	9,467	6,302	9,625	9,740	9,166
SW Pass closure, published discharge SW Pass closure, routed discharge										
		Cvcle	s 1289-12	290						
Base test, published discharge	7,276	8,193	9,453	6,875	4,870	4,469	3,208	7,73 ⁴	6,703	2,807
Base test, routed discharge SW Pass closure, published discharge	8,937	11,229	10,198	9,281	8,823	9,166	5,901	9,337	9,396	6,989
SW Pass closure, routed discharge	2,578	2,635	2 , 693	2 , 635	4,526	3,838	2,463	3,036	2,349	2,635
		Cycle	s 1303 - 13	304						
Base test, published discharge	6,245	7,906	8,651	6,932	4,469	3,495	3,036	7,448	6,760	3,266
Base test, routed discharge SW Pass closure, published discharge	9,109	10,943	9,109	9,223	7 , 505	5,958	6,588	10,083	9 ,6 82	5,443
SW Pass closure, routed discharge										~~~~
			s 1316-13	317						
Base test, published discharge Base test, routed discharge	7,219 8,995	7,849 11,114	8,193 9,625	6,989 9,396	3,781 7,276	2,979 6,187	3,208 5,614	7,104 9,281	6,760 9,682	3,609 5,156
SW Pass closure, published discharge	2,750	2,807	2,865	2,807	3,781	2,807	2,521	3,208	2,349	3,495
SW Pass closure, routed discharge	ر _ا و ح				٠٠٠ وق	2,001	29 721	3,200	2 , 349	رودرد
	7,161		s 1343 - 13 9,625	6,875	3,609	3 00%	2,865	7 076	6 ,7 03	2)127
Base test, published discharge Base test, routed discharge	9,052	7,448 11,458	11,343	9,281	6,703	3,094 6,474	5,443	7,276 9,510	9,682	3,437 6,646
SW Pass closure, published discharge SW Pass closure, routed discharge	2,922	3,208	2,979	2,922	4,354	3,781	2,406	3,036	2,635	3,552
on rate crossre, routed arbeitable	,-	-	1370-13	•	•		·	-,		• • •
Base test, published discharge	7,448	8,823	9,739	7,562	4,297	4,239	2,521	7,161	7,390	3,609
Base test, routed discharge	9,052		9,797	9,567	7,791	7,791	4,927	9,166	9,510	6,989
SW Pass closure, published discharge SW Pass closure, routed discharge	2,979	3,208	3,036	3,036	5,271	4,583	2,635	3,323	2,922	3,953
		Cycle	s 1397 - 13	398						
Base test, published discharge	7,734	9,396	9,567	7,219	5,385	5,156	2,292	7,620	7,047	4,354
Base test, routed discharge SW Pass closure, published discharge	8,937	11,171	9,510	9,396	8,708	8,937	4,526	9,567	9,281	8,135
SW Pass closure, routed discharge	3,036	3,151	3,151	3,208	5,557	5,042	1,776	3 , 495	2,807	4,411

Table 5 (Continued)

					Sta	tion				
Condition	1	3	5	13	27	29	34	40	46	52
		Cycles	1424-14	25						
Sase test, published discharge										
Base test, routed discharge										
W Pass closure, published discharge	2,406	3 2008	2 253	3,380	5,786	5,614	802	2 200	017	E 7700
W Pass closure, routed discharge	2,400	3,208	3,151	3,300	5,100	5,014	002	3,380	911	5,729
		Cycles	1451 - 14	152						
ase test, published discharge										
ese test, routed discharge										
W Pass closure, published discharge										
W Pass closure, routed discharge	2 ,7 50	3 , 036	3,151	3,151	5 , 443	5,443	974	3,151	917 	3,380
	Cyc	les 1478	3-1479-1 ¹	180-1481						
ese test, published discharge										
Base test, routed discharge										
W Pass closure, published discharge			2-2		l. (00	2 1.05	3 777	2.502	0.001	3 000
W Pass closure, routed discharge	2,979	3,380	3,266	3,323	4,698	3 , 43 7	1,776	3,781	2,234	1,089
		Cycles	1505-15	506						
ase test, published discharge										
ase test, routed discharge										
W Pass closure, published discharge										
W Pass closure, routed discharge	2,979	3,323	3,151	3,266	3 , 838	3,609	917	3,495	1,547	2 , 635

Table 6 Low and High Salinity Measurements in Base Tests and Closure Test, First and Second Years
Salinity in ppm

	·····					·			
Station	Base Test 1954 Published Discharge	1954 Routed Discharge	Closure Test, 1954 Published Discharge	Closure Test, 1954 Routed Discharge	Stat1on	Base Test 1954 Published Discharge	1954 Routed Discharge	Closure Test, 1954 Published Discharge	Closure Test, 1954 Routed Discharge
	Low S	alinity, First	Year*			High Se	llinity, First	Year**	
1 2 3 4 5 5 6 7 8 9 10 11 11 11 11 12 12 12 12 12 12 12 12 12	1954 Published Discharge	Discharge	Published Discharge	Routed	1234556789011214161181981222222222333335678394143454952355555558981234566689071	1954 Published Discharge	Discharge	Published Discharge	Routed Discher Re 496 100 134 154 100
74 75		115 115 115	115 229	115 115 115	72 73 74 75 76		1,031 1,490 917	630 401 229	115 115 115 115
10		TT2	57		Continued)			ccy	112

Base test 1954 published discharge not taken. 1954 routed discharge taken on cycles 304-305-306-307. Closure test 1954 published discharge taken on cycles 304-305-306-307. Closure test 1954 routed discharge taken on cycles 360-361-362-363.

Base test 1954 published discharge not taken. 1954 routed discharge taken on cycles 560-561-562-563. Closure test 1954 published discharge taken on cycles 560-561-562-563. Closure test 1954 routed discharge taken on cycles 749-750-751-752.

Table 6 (Continued)

Station	Base Test 1954 Published Discharge	1954 Routed Discharge	Closure Test, 1954 Published Discharge	Closure Test, 1954 Routed Discharge	Station	Base Test 1954 Published Discharge	1954 Routed Discharge	Closure Test, 1954 Published Discharge	Closure Test, 1954 Routed Discharge
	Low Sal	Linity, Second	Year*			High Sa	linity, Second	Year**	
1234556789911214161789212245628233335333341444445690235555555566666666667777777	2,120 2,922 2,292 3,349 3,036 3,380 3,552 3,495 3,495 3,495 3,497 3,036 1,005	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	Year*	6320 6320 6320 6320 6320 6320 6320 6320 6320 6320 6321 6321 6321 6321 6322 6323 6324 6325 6325 6326 6326 6326 6327 6326 6327	12345567890112341667890112345678901333333333344444490525555555566666666671277777	#igh Sa: 7,104 7,677 9,739 11,859 12,375 11,677 11,627 11	8,594 11,7000 11,744 13,000 11,744 13,000 11,744 13,000 11,744 13,000 11,744 13,000 11,744 13,000 11,745 13,979 13,520 10,427 12,445 13,979 13,520 13,426 9,625 9,567 9,3312 11,573 12,665 10,427 10,555 10,089 10,369 10,198 10,369 10,198 10,369 10,427 10,555 10,089 10,427 10,655 10,089 10,427 10,655 10,6	Year**	2,3,630,622,661,157,900,666,71,166,600,000,700,166,43,700,200,200,170,

Base test 1954 published discharge taken on cycles 1006-1007-1008-1009. 1954 routed discharge taken on cycles 1006-1007-1008-1009. Closure test 1954 published discharge not taken. Closure test 1954 routed discharge taken on cycles 1108-1110-1111.

Base test 1954 published discharge taken on cycles 1262-1263-1264-1265. Test 1954 routed discharge taken on cycles 1262-1263-1264-1265. Closure test 1954 published discharge not taken. Closure test 1954 routed discharge taken on cycles 1478-1479-1480-1481.

Table 7

Salinity Tests, 1955 Routed Discharge Hydrographs
Salinity in ppm

					St	ation				···········
Condition	1	3	5	13	27	29	34	40	46	52
				Cycles	8_0					
Dage bank		0 653				7 006	0.070	7 505	E 1112	
Base test Closure test		8,651 6,359	5,271	4,927 4,755	6,187 8,937	7,906 4,927	2,979 2,177	7,505 4,927	5,443 4,583	
Withdrawal test		5,729	5,672	2,865	10,427	5,156	286	6,302	2,807	
	Cycles 20-21									
Base test	5,213	8,307	9,281	6,015	10,885	5,156	4,927	7,390	6 , 359	6,130
Closure test	4,411	5,901		4,526	8,135	4,640	2,292	4,526	4,411	5,271
Withdrawal test	3,495	5,672	6,818	3,266	9 , 453	5,672	1,833	5,844	2,635	6,703
				ycles 4						
Base test Closure test	4,239	7,1 61		5,099	8,880	5,099	3,495	6,989	3,495	3,437
Withdrawal test	3,495 3,380	5,156 5,328	4,698	3,437 3,667	6,015 7,448	2,979 3,609	1,432 1,031	4,239 5,500	2,005 1,833	2,521 2,807
	-,-	,,,	•	•		٠, ,	, ,	-,,	, 55	
	- 1	C = 0=	_	ycles 7		1	- 1	<i>c</i>	-11	
Base test Closure test	1,490 2,234	6,187 5,156	3,208 4,812	2,922	6,474 4,239	3,094 3,151	1,490 1,719	6,073 3,667	344 5 1 6	3,781 2,463
Withdrawal test	1,021	5,156	2,463		5,55 7	2,922	1,776	4,870	229	3,437
			Су	cles 10	1-102					
Base test	1,260	4.870	1,203		5,099	2,979	115	3,724	401	1,089
Closure test	2,349	4,068	4,469	2,120	3,437	2,234	630	2,635	458	2,234
Withdrawal test	802	4,010	1,776	1,833	4,297	2,234	458	3,151	115	1,547
			<u>С</u> у	cles 12	8-129					
Base test	1,719	3,781			2,807	1,432	115	3,323	2,005	115
Closure test Withdrawal test	2,635 1,604	3,667	3,380 2,062	1,490 2,005	2,234 2,693	1,661 1,031	516 115	2,234 3,151	1,776 1,891	458 172
	_,	3,1	•	•		, -5.		J y /	-, 0)-	-1-
				cles 15						
Base test Closure test	2,062	3,609			1,432	687 687	917	3,094	2,521	115
Withdrawal test	2,521 1,719	3,266 3,208	2,521 1,547		1,089 1,260	401	9 17 5 7 3	2,005 2,406	1,891 1,891	344 115
	,,,,	-,					, , ,		,	
Deen test	0.700	2 001		cles 18		1.50	r3 (0.000	0.1:60	
Base test Closure test	2,120 1.719	2,922	1,547 1,661	1,604 1,719	7 45 458	458 286	516 516	2,292	2,463 2,349	229 115
Withdrawal test	1,719		1,089	1,318	516	286	458	1,833	1,833	115
Cycles 209-210										
Base test	630	1,719	1,719	917	401	286	172	1,547	286	172
Closure test	859	1,948	630	344	286	286	344	802	229	115
Withdrawal test	57 3	1,719	1,031	344	286	286	172	1,432	172	172

Table 7 (Continued)

	····	· · · · · · · · · · · · · · · · · · ·			Q+c	tion					
Condition	1	3	5	13	27	29	34	40	46	52	
											
			<u>C</u> y	cles 236	o - 237						
Base test	859	1,604	1,375	630	229	115	115	1,089	735	115	
Closure test Withdrawal test	859 802	1,547 1,260	458 1 , 089	687 5 7 3	172 172	115 1 7 2	172 172	859 5 7 3	1,260 802	115 172	
Wildianar Cost	002	- ,	2,0 0)	713	I	-1-	1	713	002	-,-	
Cycles 249-250											
Base test	802	1,490	1,146	630	17 2	1 7 2	2 29	9 7 4	917	115	
Closure test Withdrawal test											
withdrawai test											
			Су	cles 263	3 - 264						
Base test	5 7 3	1,260	1,146	5 7 3	172	229	115	802	5 7 3	115	
Closure test	802	1,260	573	1,031	115	115	115	344	917	115	
Withdrawal test	5 7 3	974	1,146	458	229	17 2	229	5 1 6	5 7 3	172	
			Cycles	2 7 9-280) - 281-282	2					
Base test	516	1,375	1,089	458	17 2	229	115	802	458	115	
Closure test	802	1,260	1,146	687	229	1 7 2	172	516	401	172	
Withdrawal test	401	1,031	802	401	11 5	115	115	5 7 3	344	115	
			Су	cles 290	-291						
Base test	5 1 6	1,604	1,432	630	344	17 2	229	802	5 7 3	115	
Closure test	7 45	1,146	1,146	687	115	172	115	630	458	115	
Withdrawal test	458	630	5 7 3	458	17 2	17 2	115	516	458	172	
			Су	cles 303	3-304						
Base test	5 7 3	1,661	1,432	603	229	229	115	687	630	172	
Closure test											
Withdrawal test											
			Су	cles 317	7 - 318						
Base test	5 7 3	2,120	1,661	802	115	115	115	745	687	115	
Closure test	687	802	7 45	687	229	229	172	7 45	917	172	
Withdrawal test	5 1 6	687	630	5 1 6	17 2	172	17 2	516	5 7 3	115	
			Су	cles 344	<u>-345</u>						
Base test	687	2,234	1,833	630	115	115	115	1,318	974	115	
Closure test	745	917	7 45	802	286	229	172	802	859	172	
Withdrawal test	458	458	5 7 3	401	5 7	5 7	172	458	516	115	
			Су	cles 371	<u>-37</u> 2						
Base test	917	2,750	2,463	1,375	286	286	115	2,177	516	115	
Closure test	687	974	859	687	401	286	229	802	5 1 6	172	
Withdrawal test	516	458	458	401	115	172	115	5 7 3	458	115	
			<u>C</u> y	cles 398	3-399						
Base test	974	2,292	2,693	1,661	573	516	115	2,863	859	115	
Closure test	516	687	687	745	401	344	172	630	458	229	
Withdrawal test	458	458	516	516	172	172	115	516	401	115	

					St	ation			- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	
Condition	1	3	_ 5	<u>13</u>	27	29	34	40	46	52
			Сv	cles 425	5-426					
Base test	5 7 3	3 , 552	2,5 7 8		745	630	115	2 , 5 7 8	5 7 3	229
Closure test	401	802	687	630	458	401	172	630	172	229
Withdrawal test	401	5 7 3	401	344	172	115	115	458	458	115
			Су	cles 452	2 - 453					
Base test	2,062		4,755		1,146	917	286	4,068	2,349	5 7 3
Closure test Withdrawal test	5 7 3 344	687 401	630 401	688 286	401 516	401 344	172 115	5 7 3 286	573 229	229 115
	J					J				
Dage togt	ລຸ ໄປລອ	7 600		cles 479		7 604	850	E 208	2 266	1 202
Base test Closure test	3,437 5 1 6	687	6 ,01 5 5 7 3	3,427 5 7 3	2,062 1,604	1,604 974	859 115	5,328 516	3 , 266 630	1,203 458
Withdrawal test	286	40i	344	286	2 ,7 50	687	401	401	286	172
			Су	cles 506	5 <u>-507</u>					
Base test	4,239	8,364	7,620	5,500	3,896	2,922	1,490	5,958	5,099	2,349
Closure test Withdrawal test	5 7 3 4 01	802 573	630 401	5 7 3 458	3,724 3,437	3,437 2,234	229 1,203	630 802	5 7 3 458	1,604 917
Withdrawar test	401	713				Z, Z, Z	1,203	002	4,70	9+1
				cles 53					_	_
Base test Closure test	5 ,7 29 5 7 3	8 ,7 65 802	6,302 630	5 , 786 5 7 3	4,870 4,182	4,354 5,2 7 1	2,406 1,203	6,760 745	5 ,67 2 344	3,609 3,724
Withdrawal test	745	7 45	5 7 3	745	5,213	4,583	3,036	1,490	745	2,750
			Су	cles 560	0-561					
Base test	6 , 359	9,510		6,416	4,812	4,640	3,380	7,104	6 ,7 03	4,068
Closure test	687	802	687	630	5,385	5,55 7	2,979	1,146	573	4 ,7 55
Withdrawal test	1,203	1,604	974	1,203	3,781	3 , 552	4,068	2 , 865	1,203	1,547
			<u>C</u> y	cles 58	7- 588					
Base test	7,219		8,135		4,698	3,781	3,036		6,932	
Closure test Withdrawal test	802 1,776	1,146 1,661	802 1,661	745 2,062	5,55 7 2,463	5,328 3,838	3,896 4,182	2,177 3,323	630 1 ,77 6	4,927 1,833
	,,,	•	·	cles 600	•		•	.,	* ' '	•
Done tout	7 560	0 /150		7,219		ار عدار	2 Q2Q	7,963	7 600), 10E
Base test Closure test	7,502	9,473			4,503	4,374	3,030	1,903	7,020	
Withdrawal test										
		<u>c</u>	ycles 6	11-612-6	613-614-	615				
Base test	7,562	9,625	8,708	7,562	5,213	4,583	3,724	7,562	8,021	4,354
Closure test Withdrawal test	1,031	1,432	1,031	1,031	4,125	4,755	3,838	2,292	630	4,640
HIMMICHAIL CESC	≟ ڪروڪ	2,710	•	•		J, 200	+,010	ا د+ود	ر نے وید	رعد و ع
		0 0		cles 64		. /		c	1 1 6-	1 (1 -
Base test Closure test Withdrawal test	5,786 1.031	8,708 1,604	9,052	6,818 859	5,729 4.640	5,156 5,042	1,719 1,318	6,760 2,521	4,469 286	4,640 5,55 7
Withdrawal test	3,036	2,635	2,807	2 , 979	3,724	3,495	2,349	3,437	3,094	2,521
				(Contin						

Table 7 (Continued)

					st	ation				
Condition	1	3	5	13	27	_29	34	40	46	52
<u>Cycles 668-669</u>										
Base test Closure test Withdrawal test	4,927 1,089 3,094	7,677 1,604 3,151	6,760 1,203 3,151	5,385 630 3,266	5,213 4,411 3,437	4,870 4,125 3,208	3,380 1,661 3,667	6,073 1,776 3,609	4,125 286 3,437	4,812 5,557 2,578
			Cycles	680-681	L-682-68	3				
Base test Closure test Withdrawal test	1,490 3,437	1,719 3,380	1,318 3,094	1,490 3,208	4,010 4,984	3,781 3,151	2,865 3,898	1,891 3,724	3 ¹ / ₄ 3 , 323	5,213 2,750
			Су	cles 695	- 696					
Base test Closure test Withdrawal test	5,786 1,719 3,495	7,276 1,776 3,609	6,359 1,3 7 5 3,036	6,015 1,661 3,667	4,640 4,526 4,870	4,411 3,667 3,323	3,495 3,323 4,068	6,073 2,005 4,016	5,672 974 3,609	4,812 5,271 3,094
			<u>С</u> у	cles 710) -711					
Base test Closure test Withdrawal test	5,844	7, 333	6,359	5,786	4 , 755	4,411	3,323	6,760	5 , 099	4,469
			Су	cles 722	2 -7 23					
Base test Closure test Withdrawal test	5,385 1,948 3,437	7,161 1,833 3,323	6,760 1,604 3,208	5,729 1,719 3,437	4,698 3,495 4,125	4,239 3,268 2,922	2,979 2,521 3,495	5,844 2,406 3,838	4,755 1,203 3,437	3,208 3,036 1,833
			Су	cles 749	-75 0					
Base test Closure test Withdrawal test	3,896 1,3 7 5 3,552	6,474 1,891 3,609	3,437 1,547 3,437		3,151 2,922 3,437	2,865 2,234 2,234	917 974 1,833	5,213 2,177 3,781	2,177 458 3,667	1,776 2,120 516
			<u>С</u> у	cles 776	5-777					
Base test Closure test Withdrawal test	859 859 2 , 463	5,042 1,948 3,667	974 2,005 3,495	1,661 1,719 3,266	2,750 2,750 2,865	2,349 2,177 2,578	630 68 7 802	4,354 1,948 3,495	115 115 2 , 693	2,635 2,865 1,833
			Сy	cles 803	<u>-804</u>					
Base test Closure test Withdrawal test	516 516 2,177	3,323 1,719 3,266	2,578 1,490 3,208	1,375 1,203 2,750	1,719 1,948 2,463	1,776 1,719 1,490	57 172 172	1,547	172 115 2,922	974 1,203 516
				cles 830						
Base test Closure test Withdrawal test	917	3,036	745 	1,318	1,203	1,318	115	2,234	1,604	229

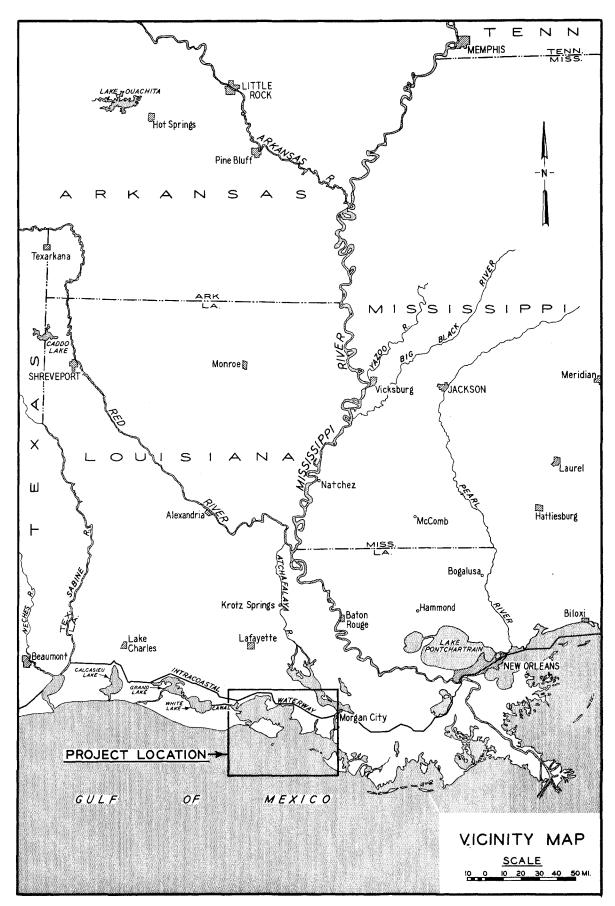
Table 8

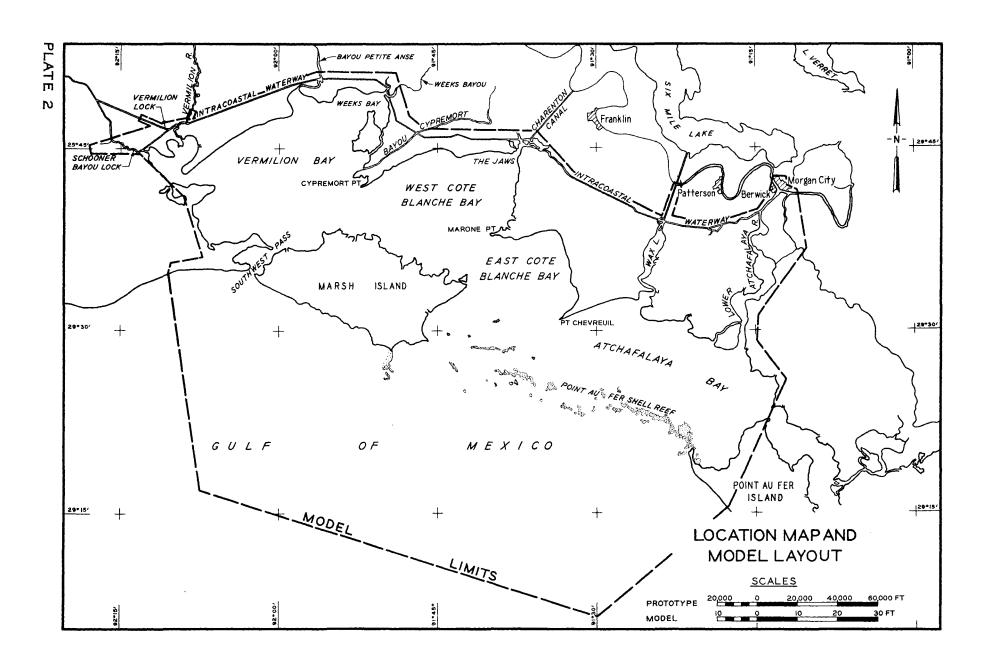
Hydrographs

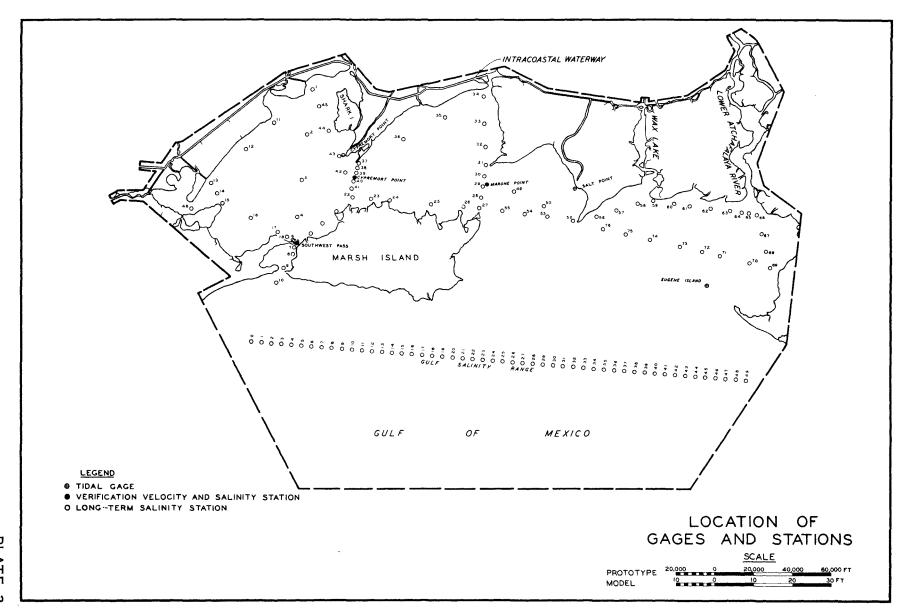
Hurricane Rainfall of September 1947

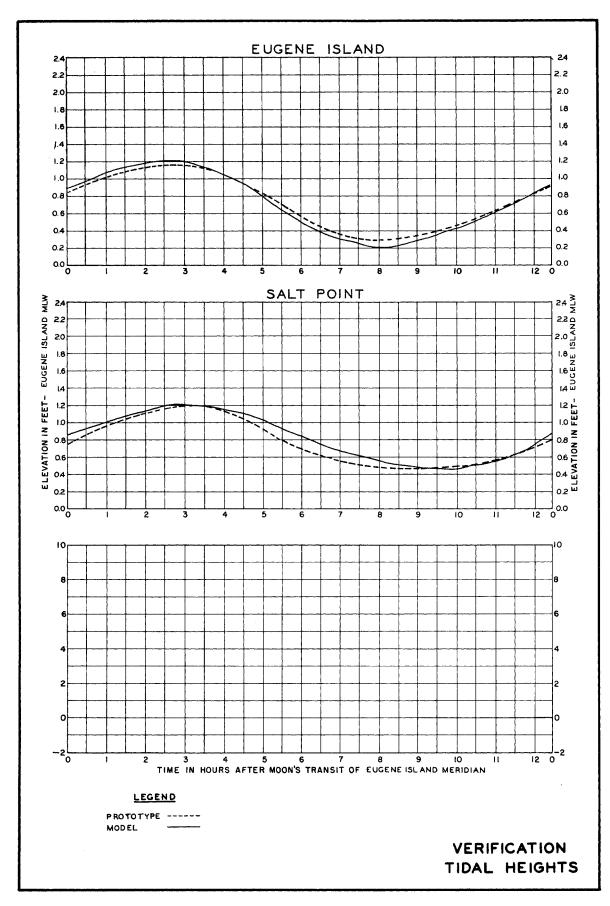
Discharge in cfs

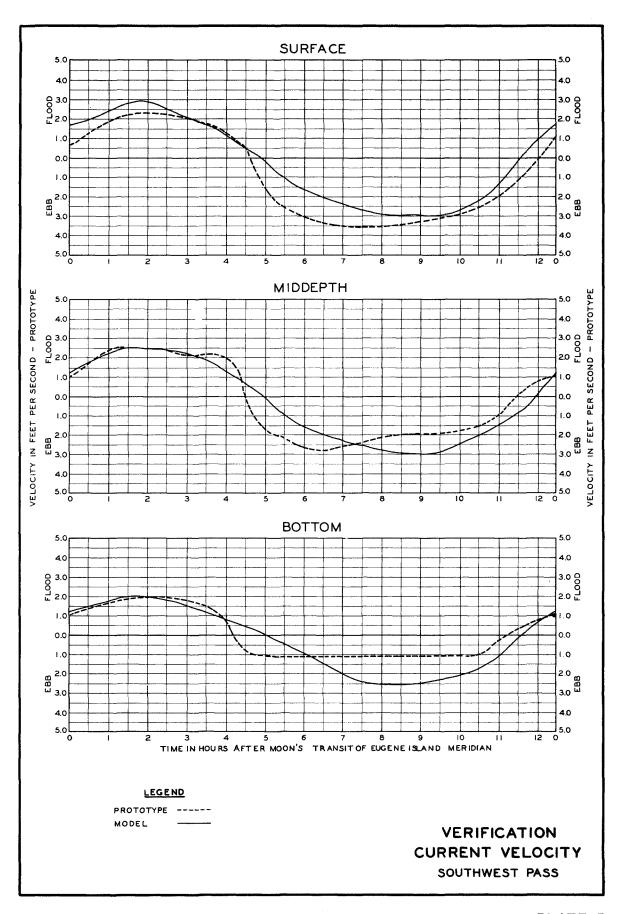
	Atchafala	aya River		Weeks Bayou,	Bayou	Vermilion
Day	Wax Lake	Morgan City	Bayou Teche	Cypremort Bayou, and Bayou Carlin	Petite Anse	River Basin
20	13,700	54,600	529	859	0	114
21	13,000	51,800	512	690	0	130
22	12,900	51,400	1,040	2,030	Ο	278
23	12,200	48,900	428	475	0	147
24	11,800	47,400	343	261	0	130
25	11,500	45,900	307	168	0	151
26	11,200	44,800	288	122	0	147
Avg	12,328.6	49,257.1	492.4	657.9	0	156.7

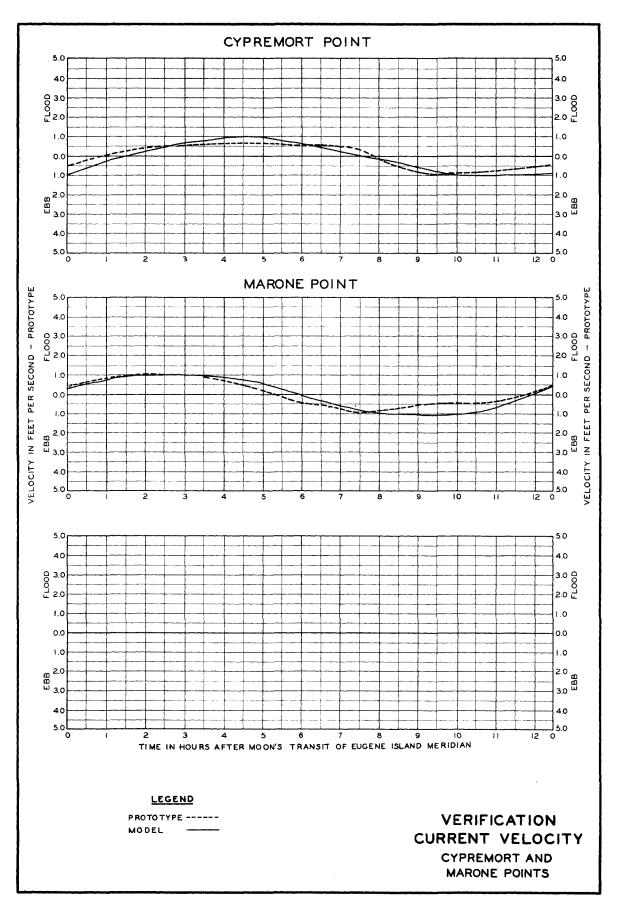


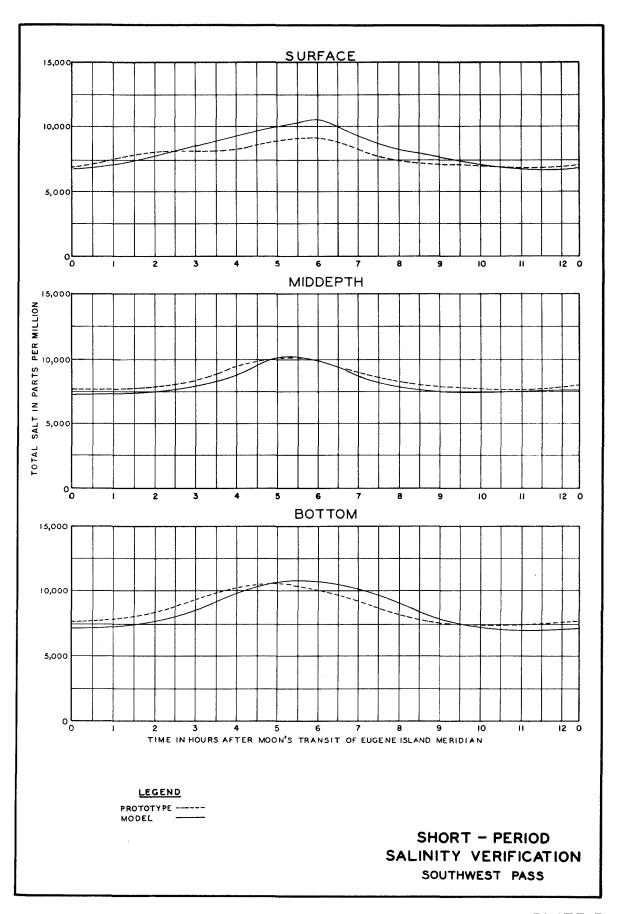


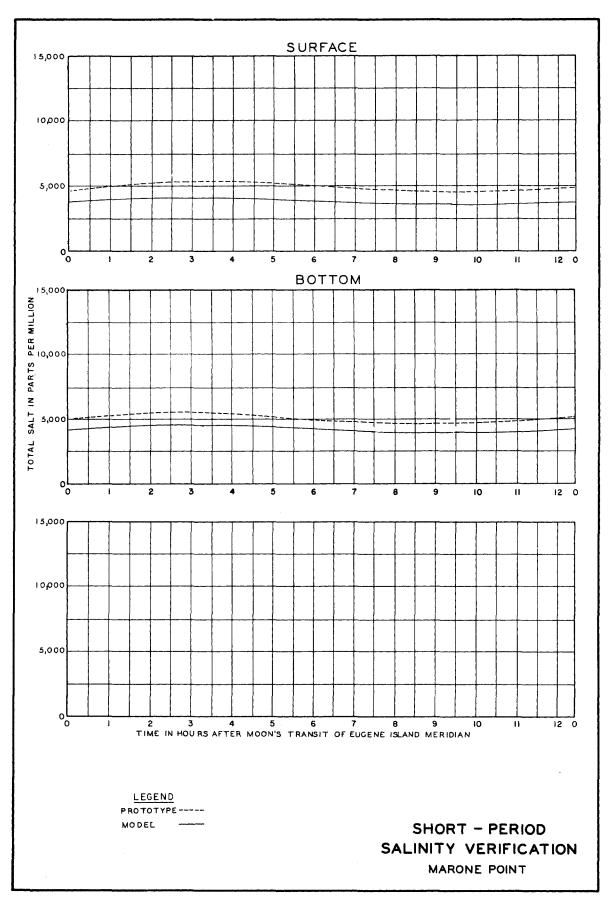


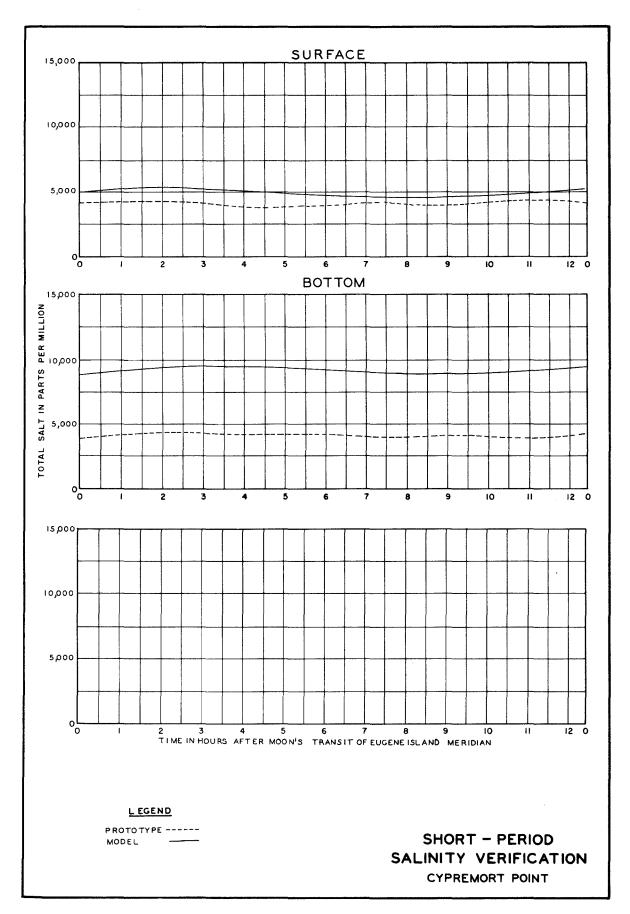


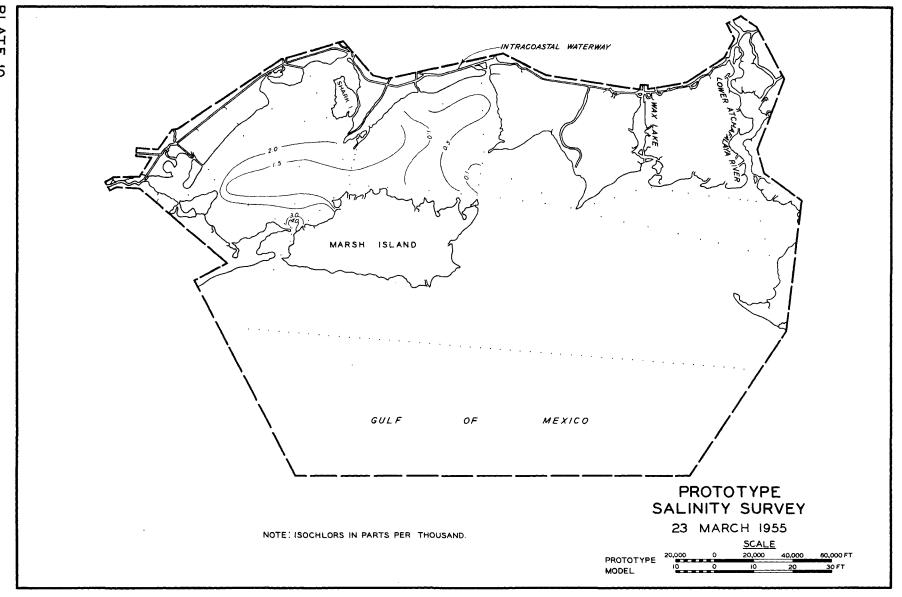


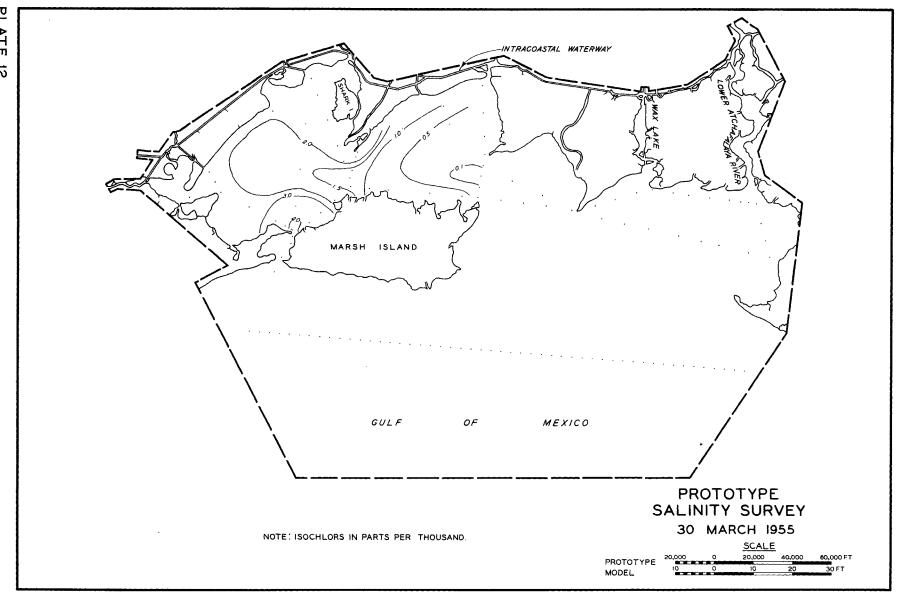


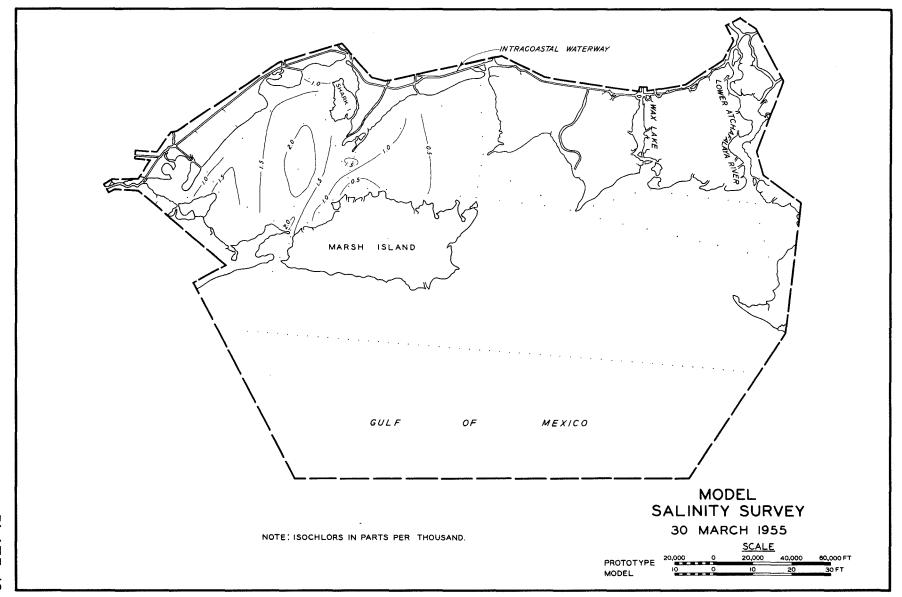


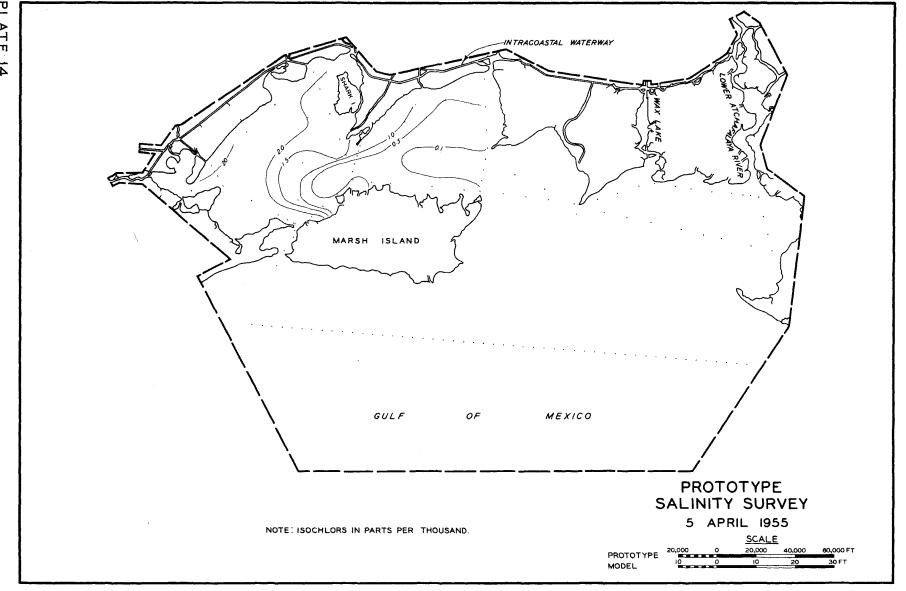


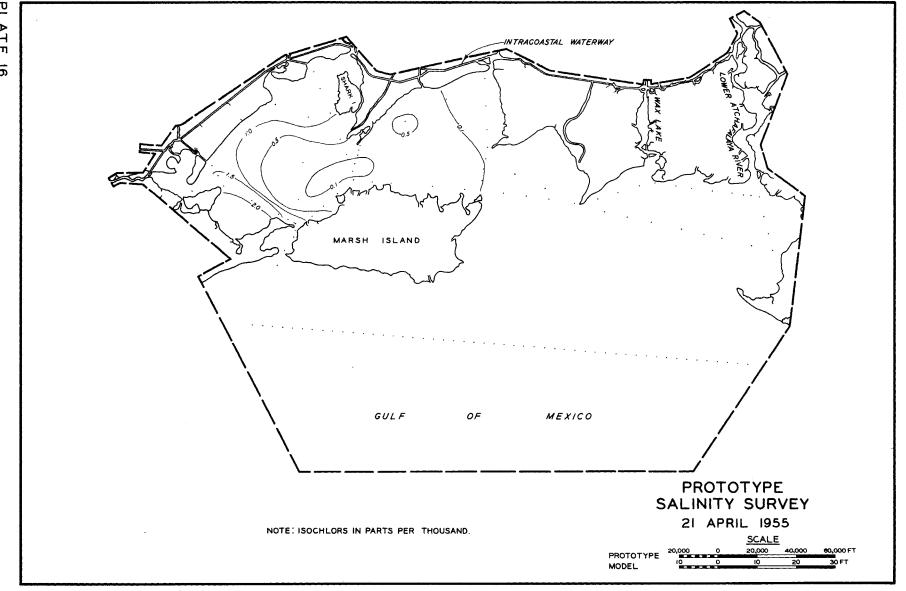


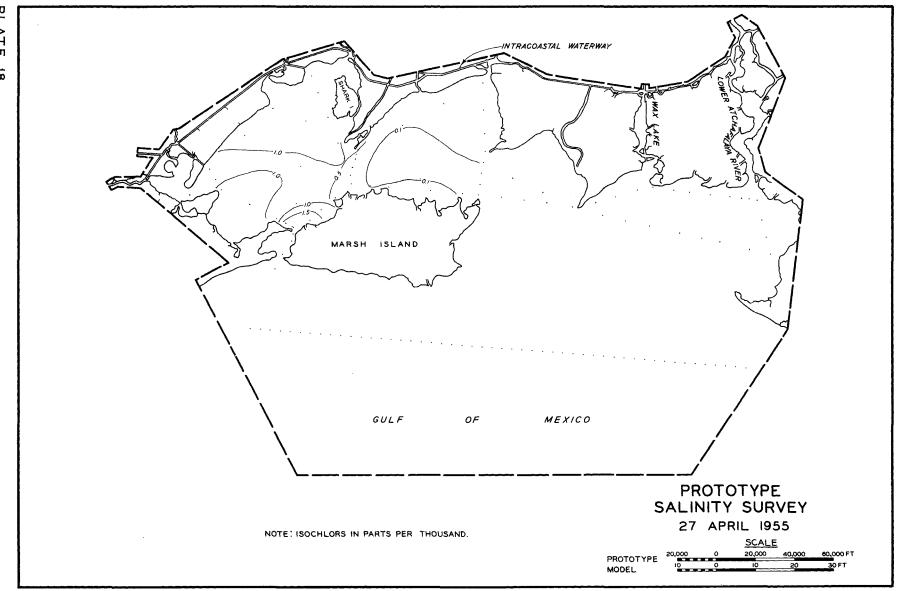


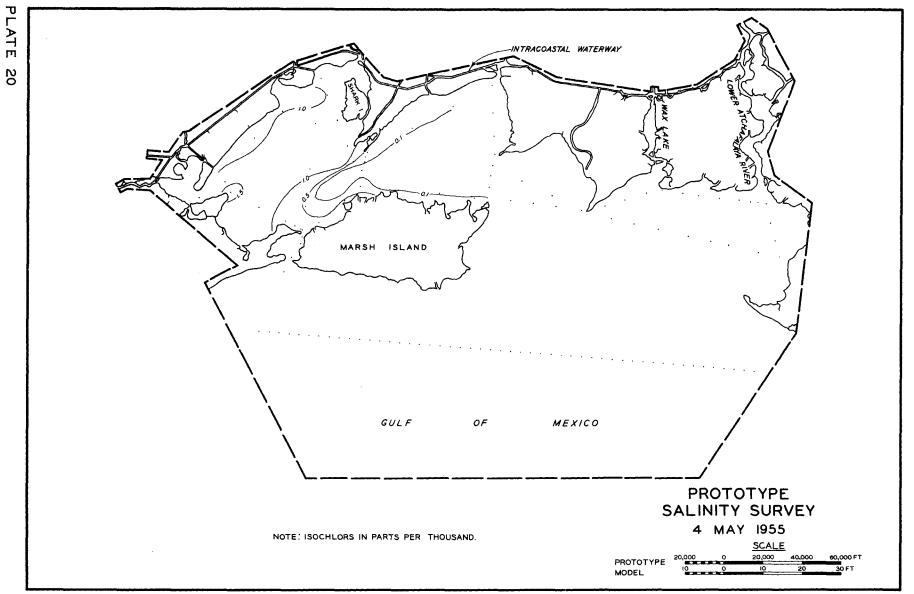


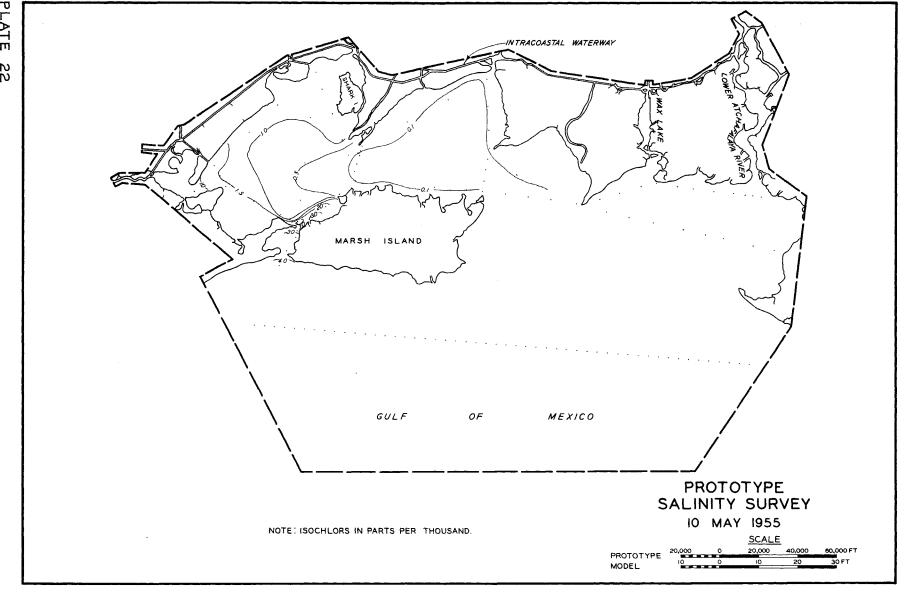


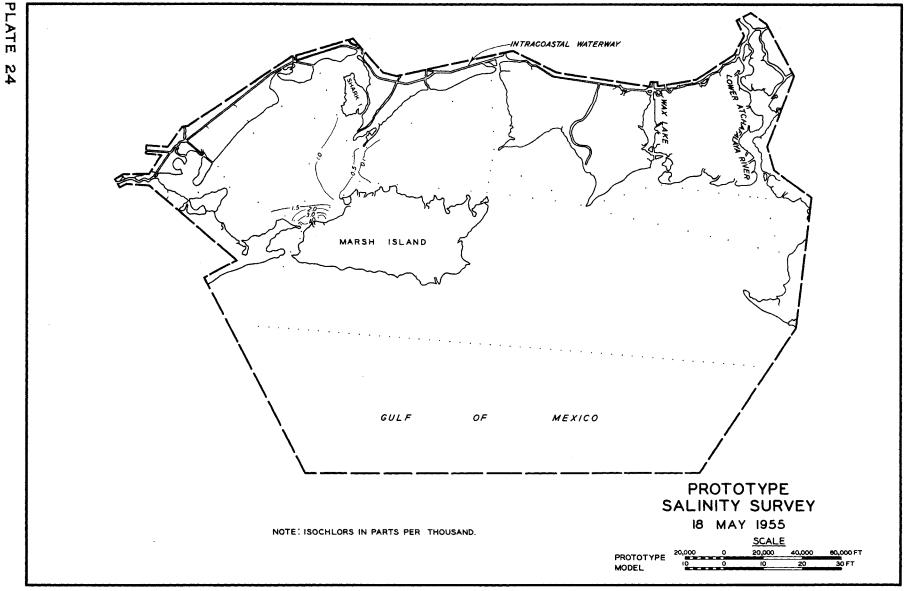


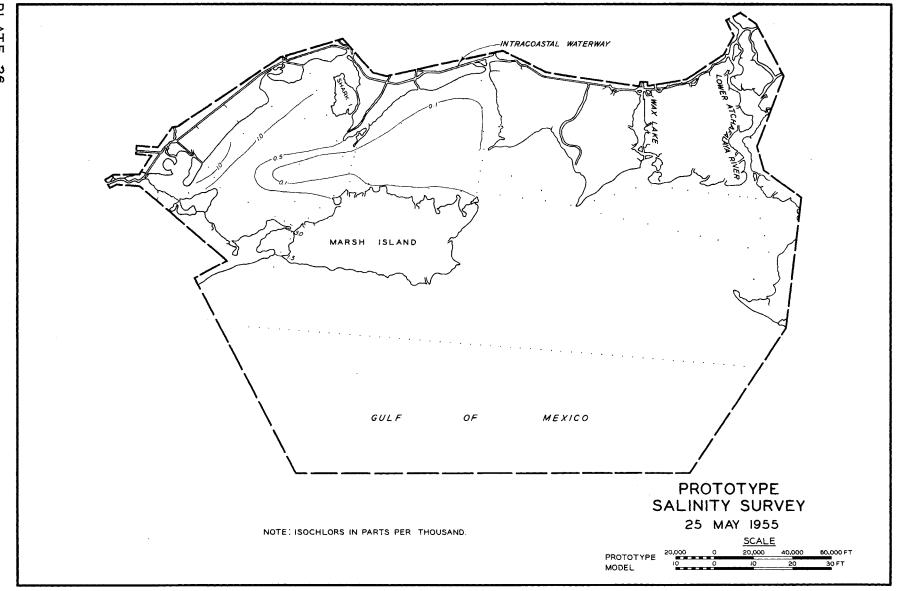


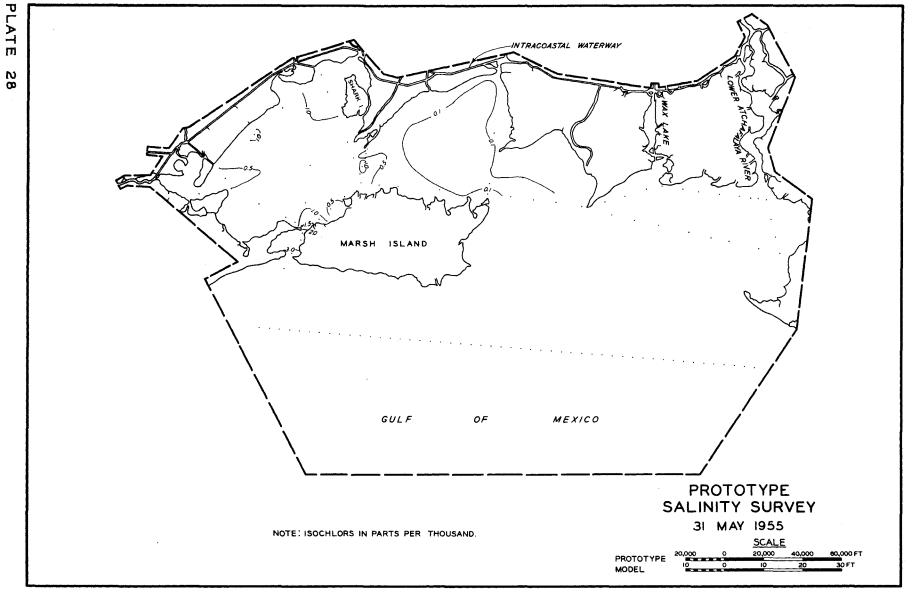


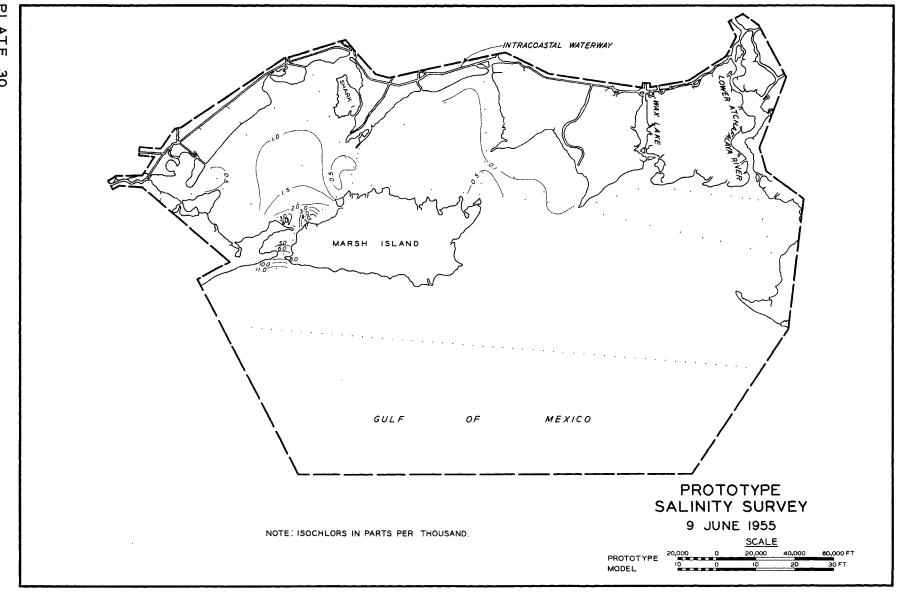


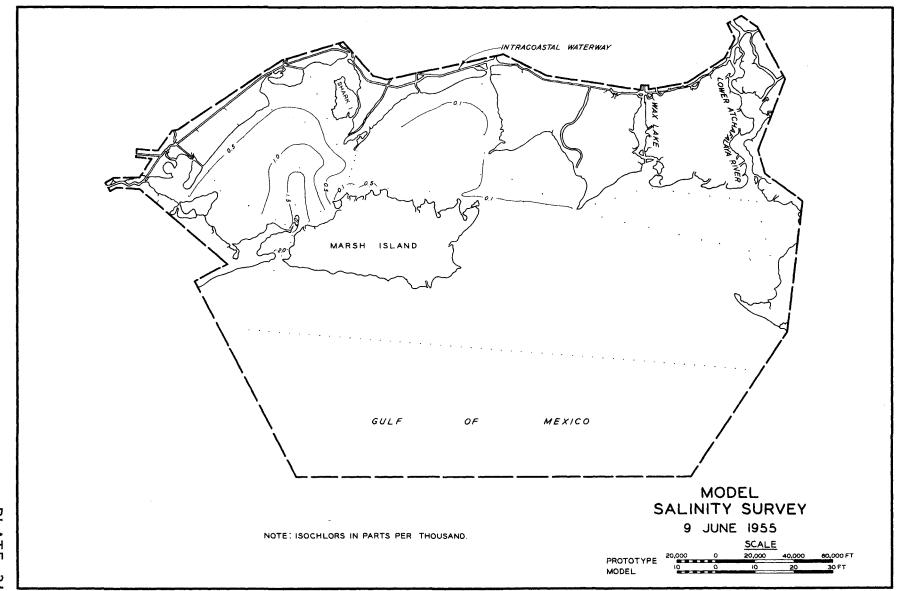


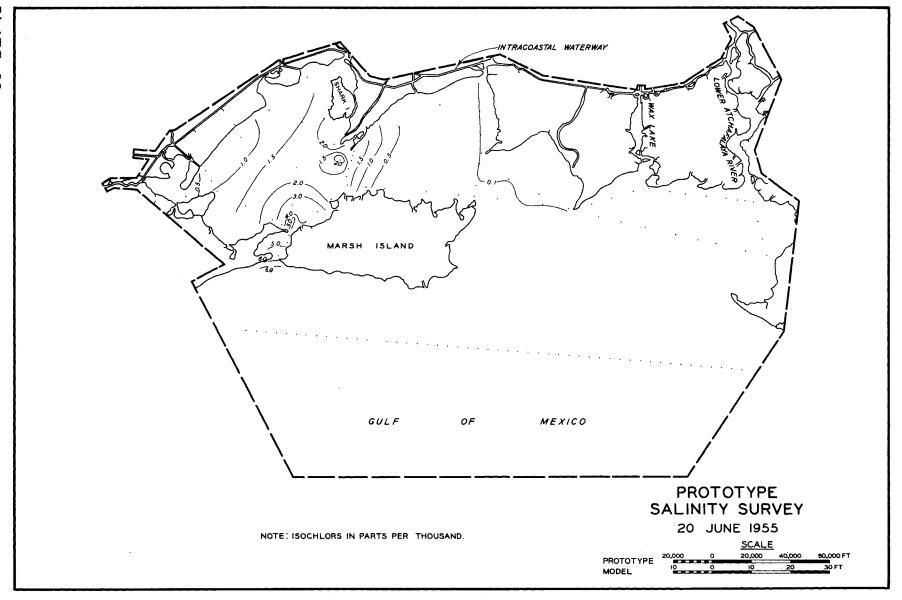


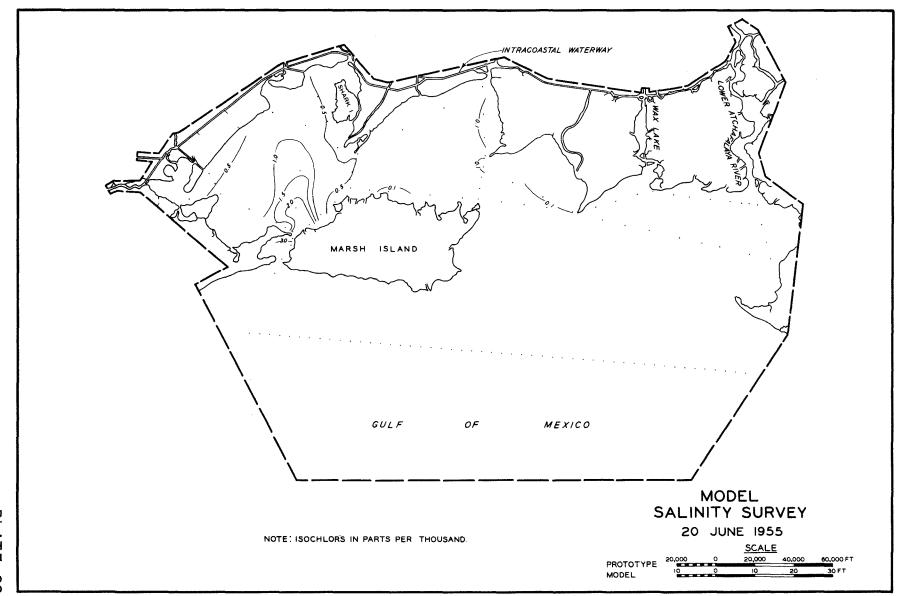


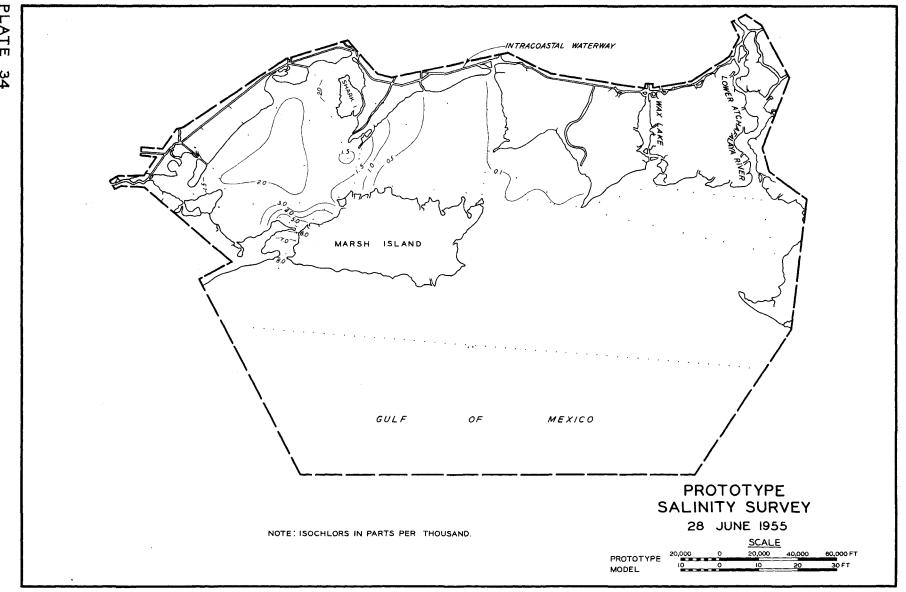


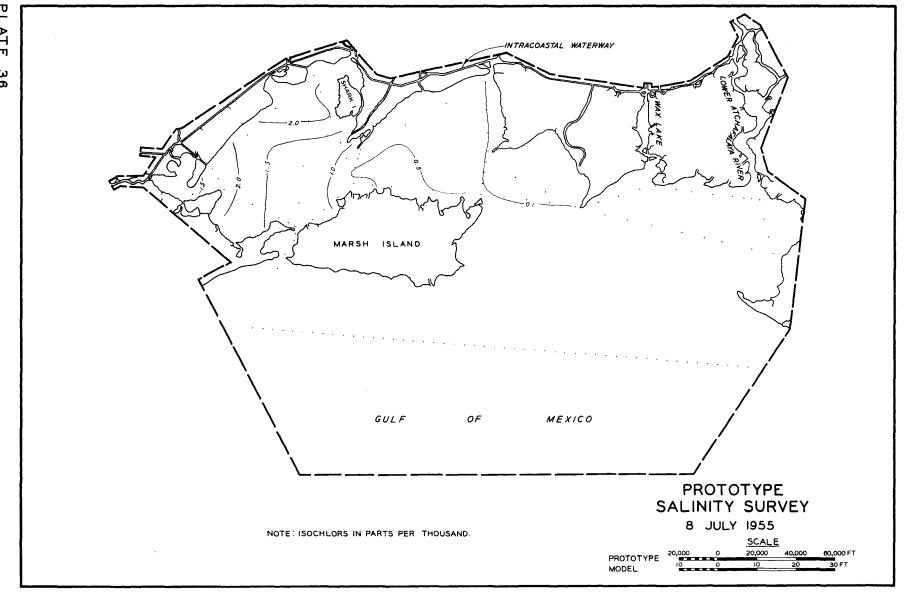


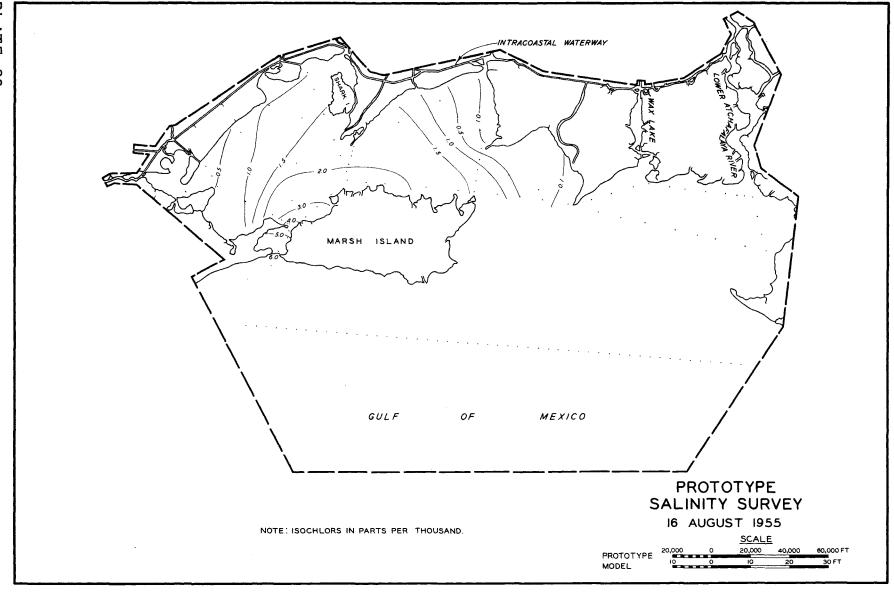


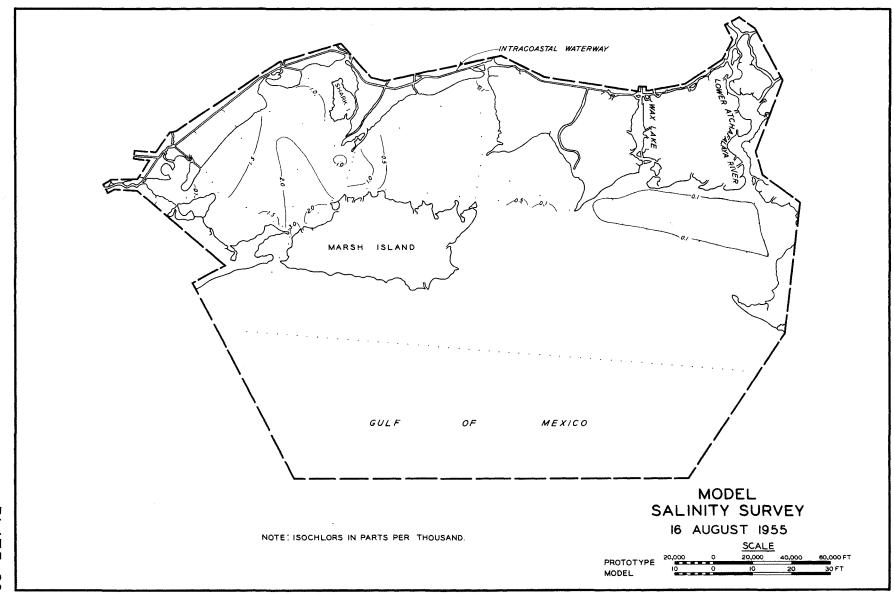


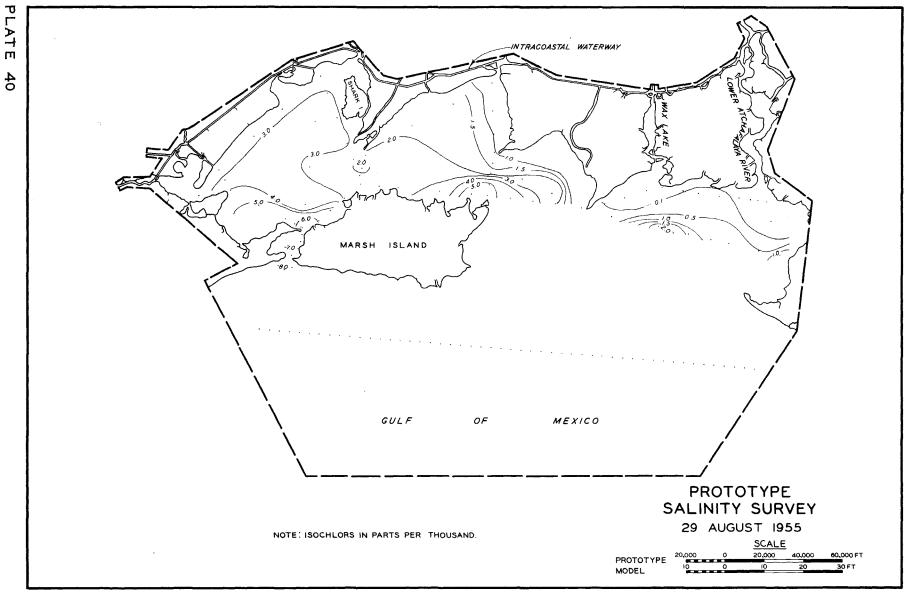




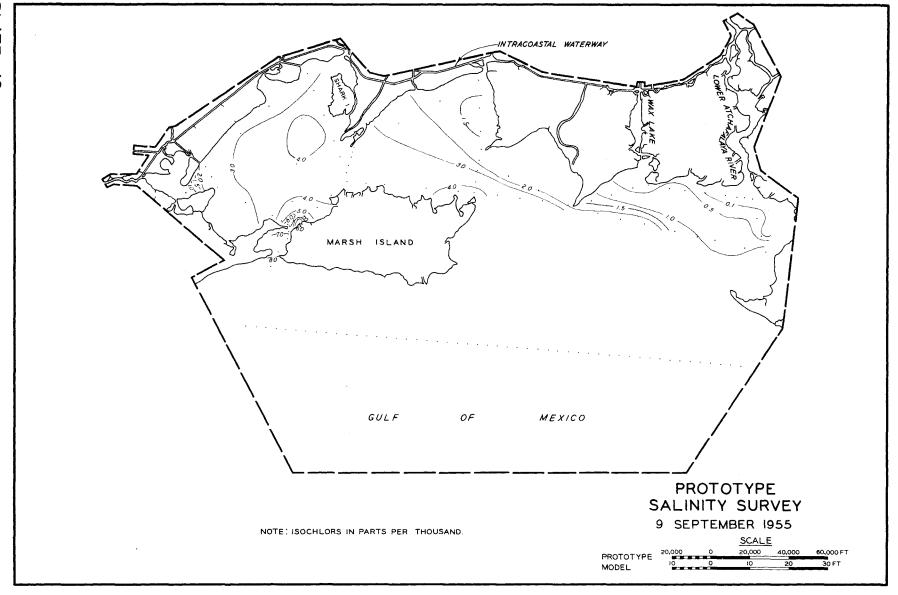


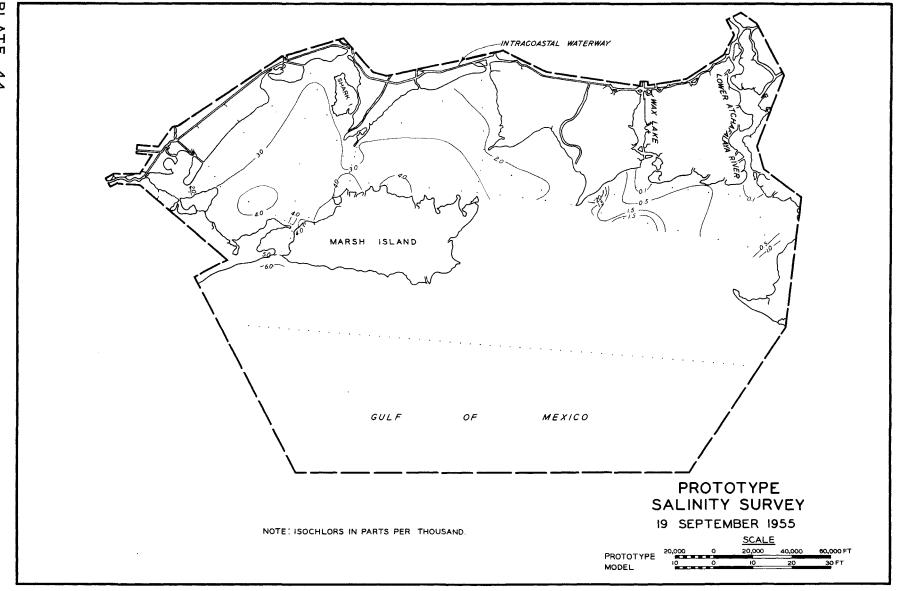




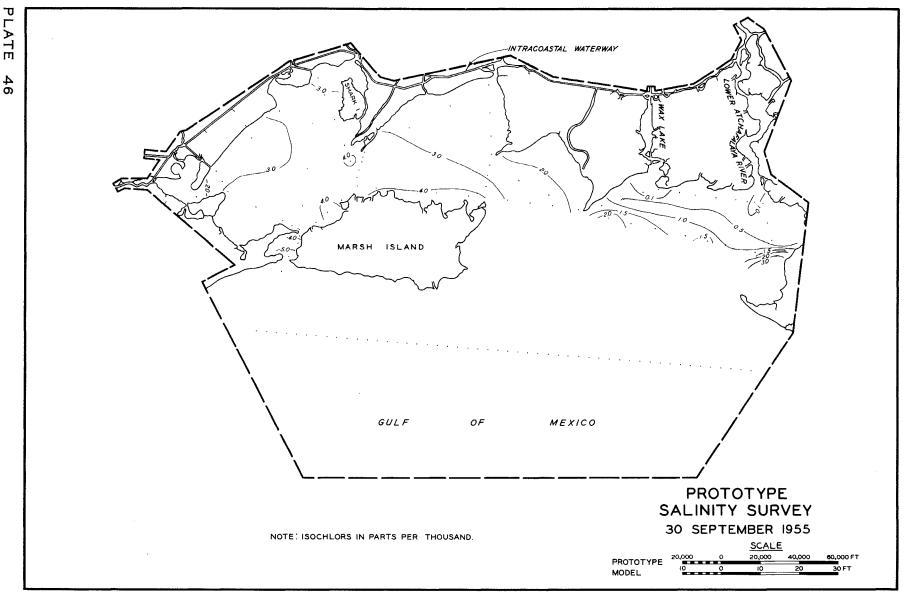


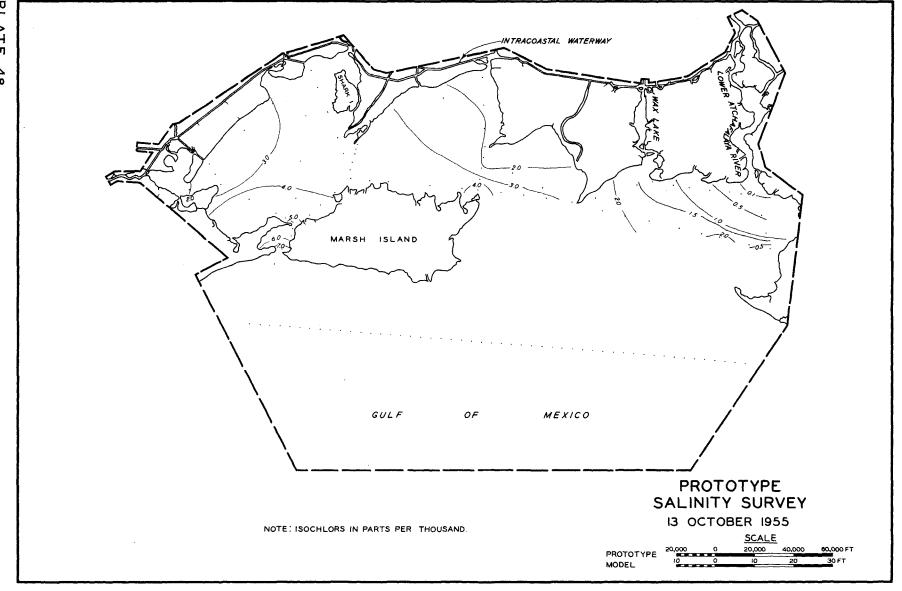
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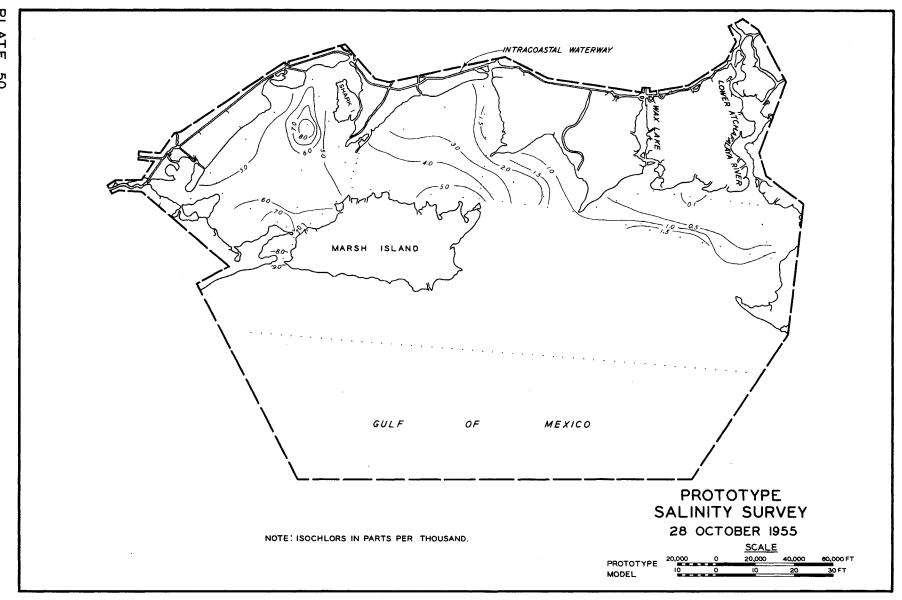


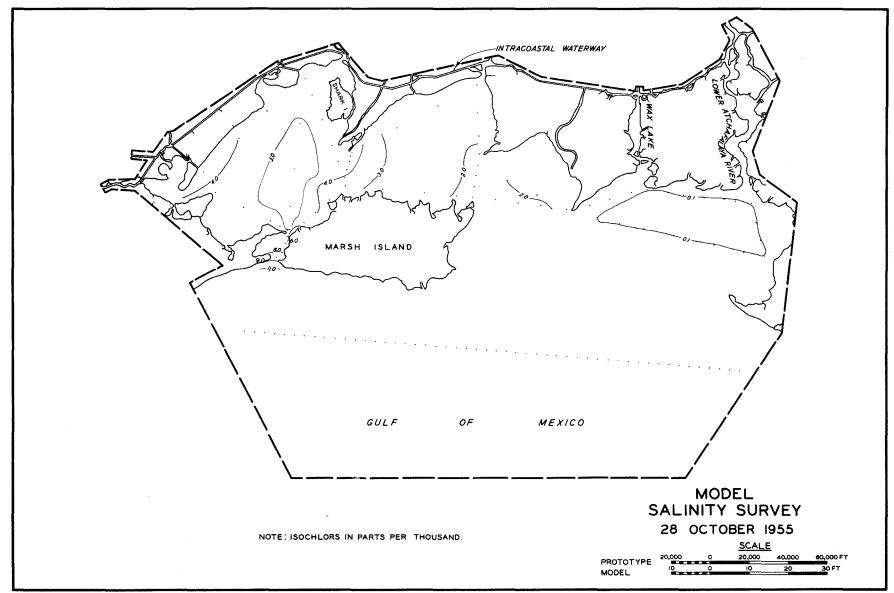


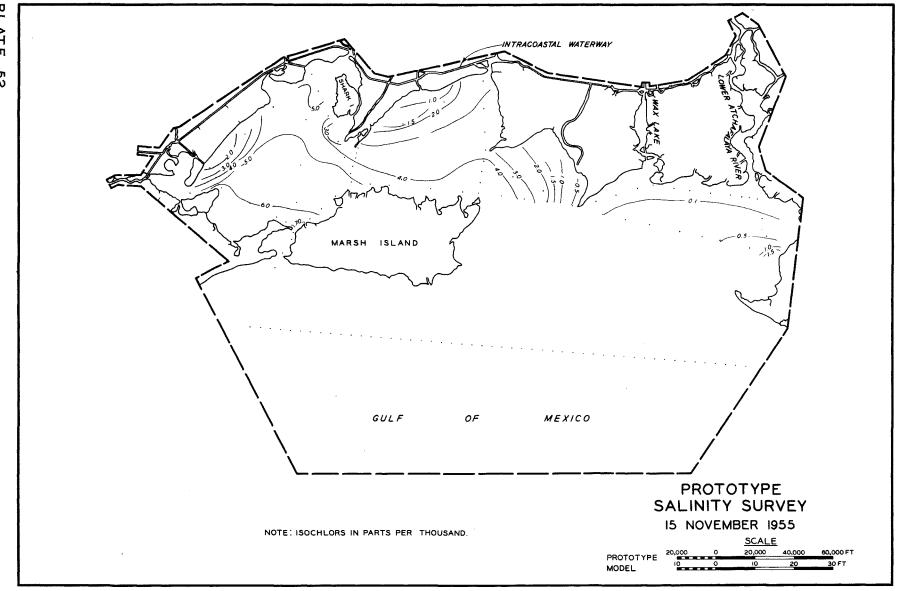
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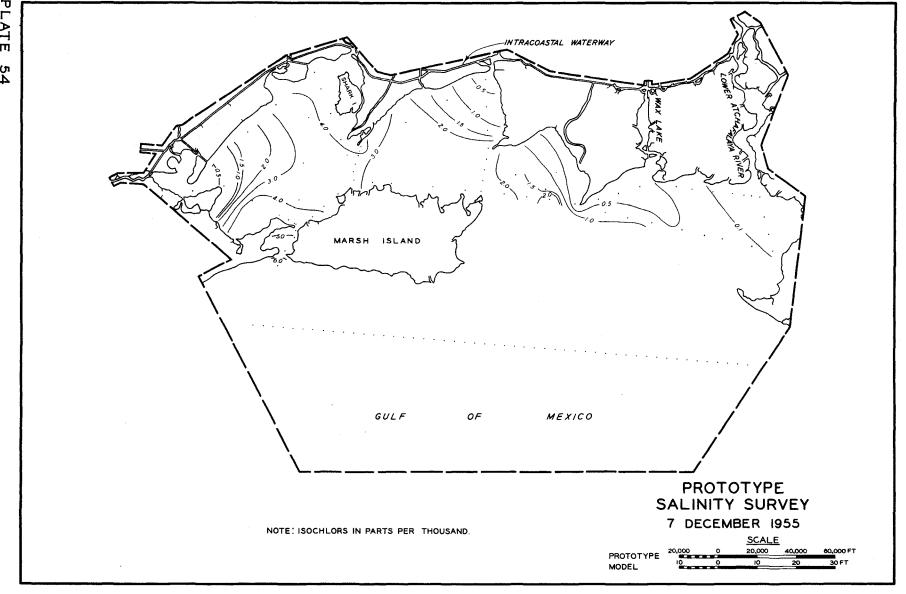


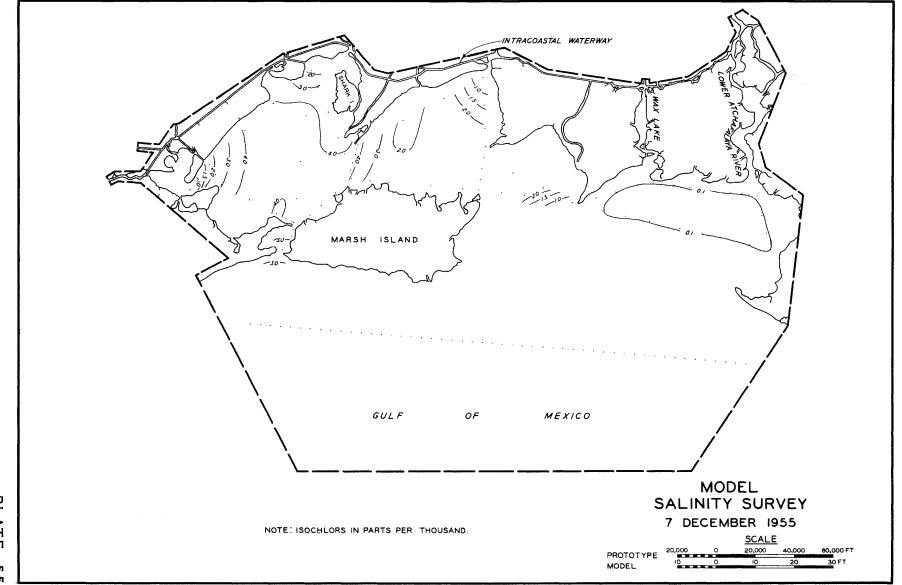


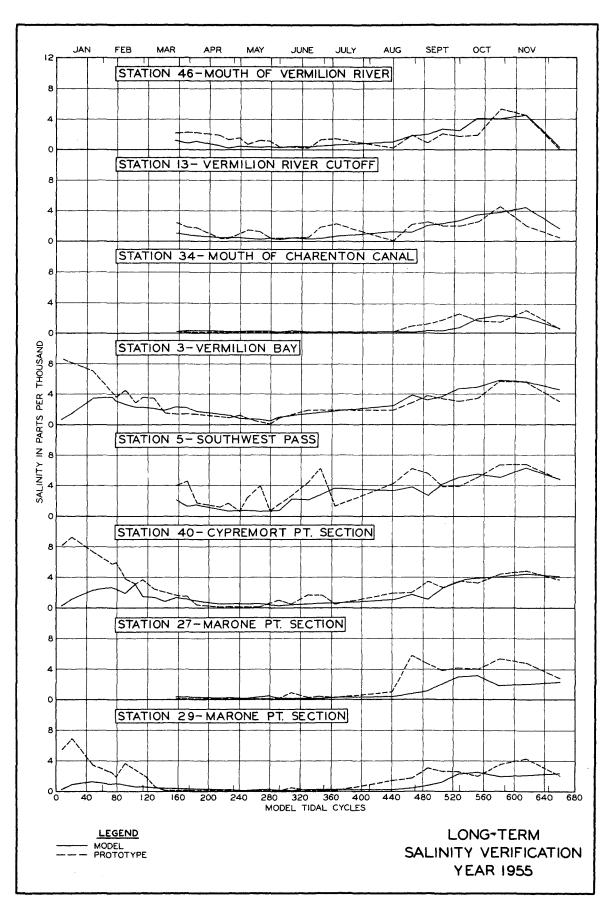


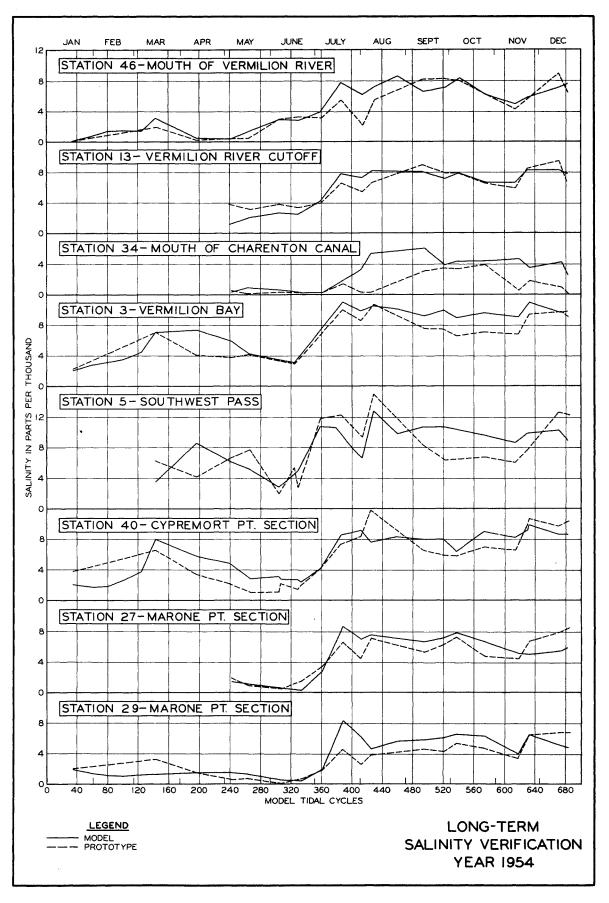


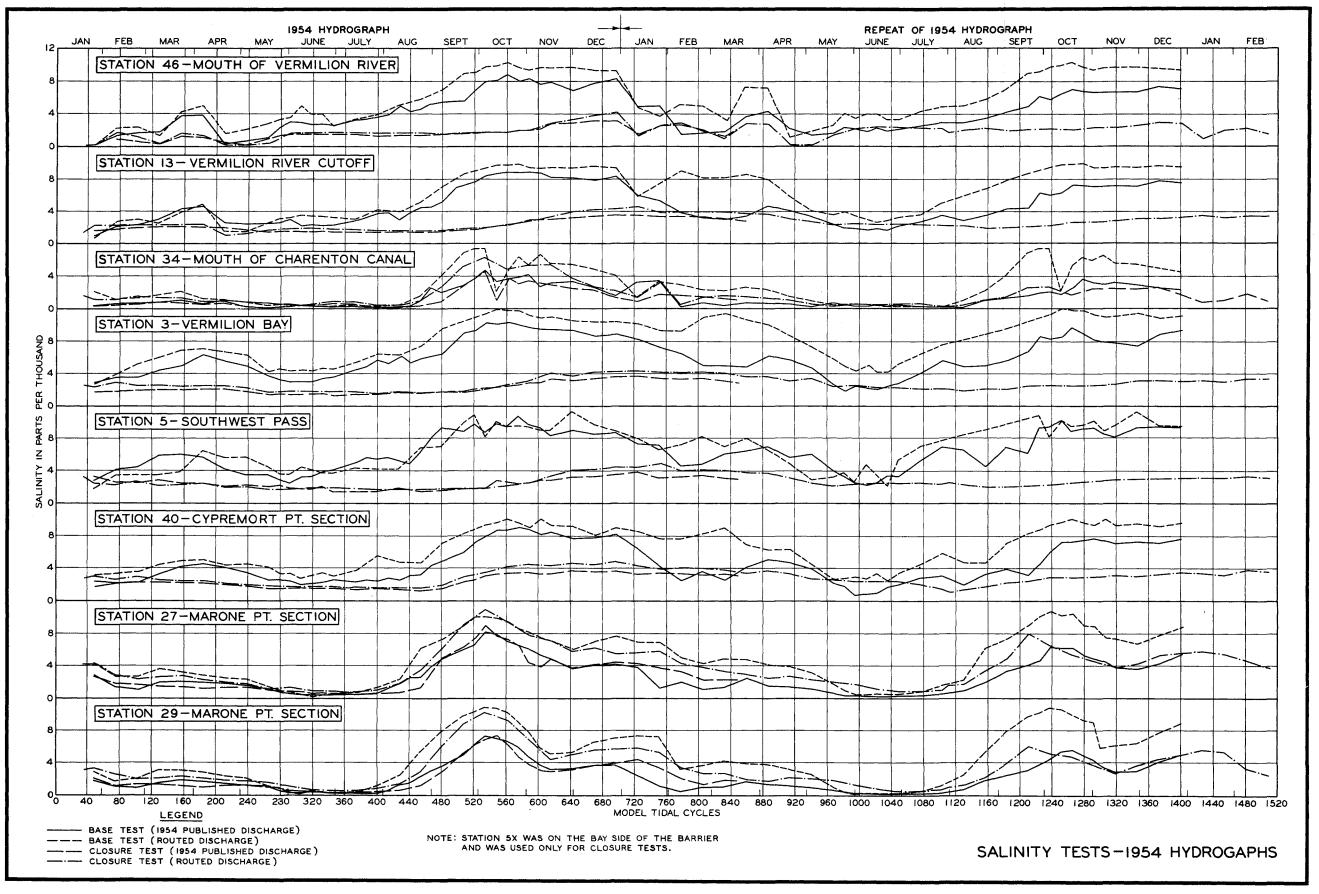


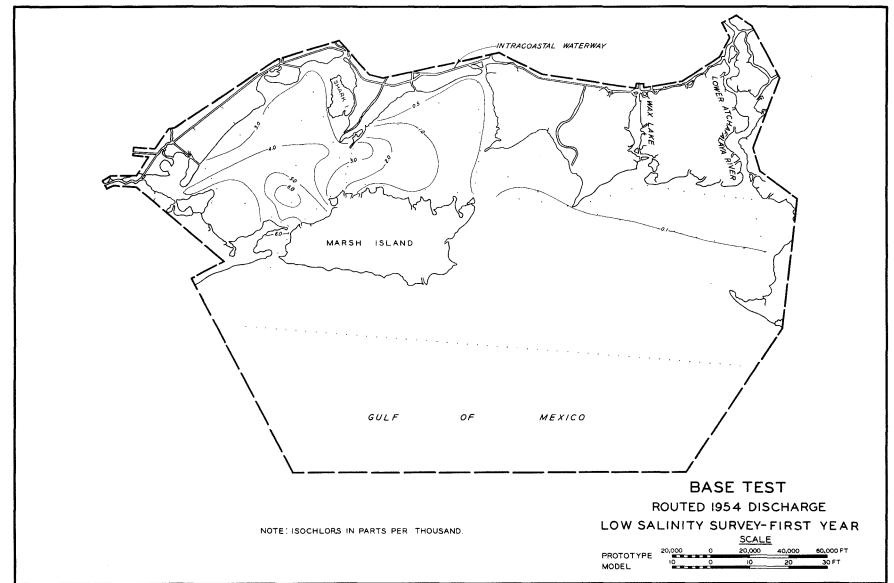


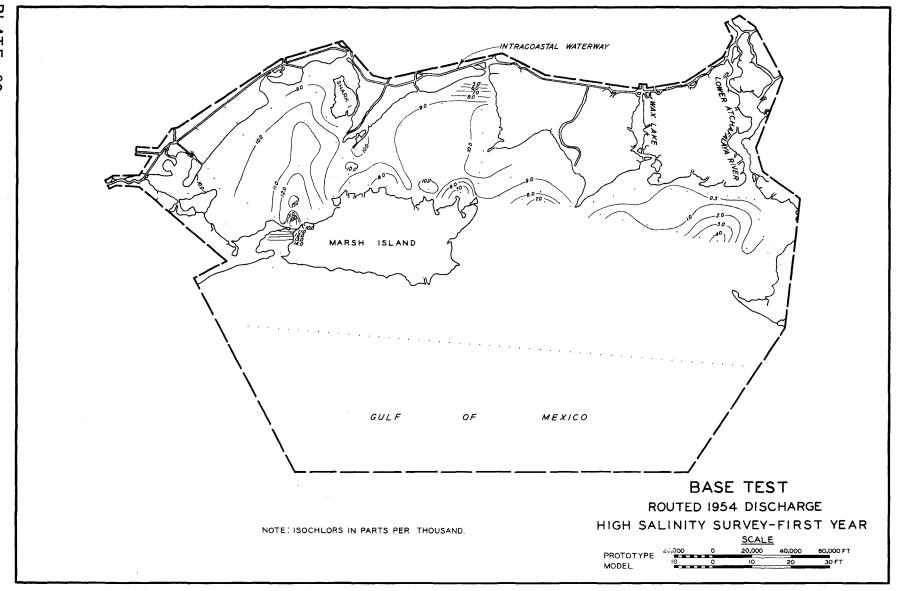


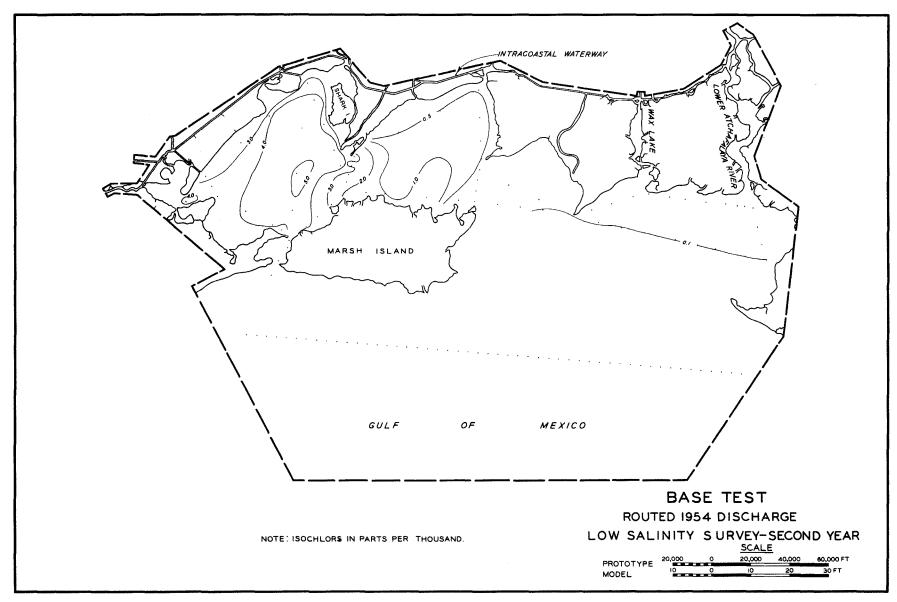


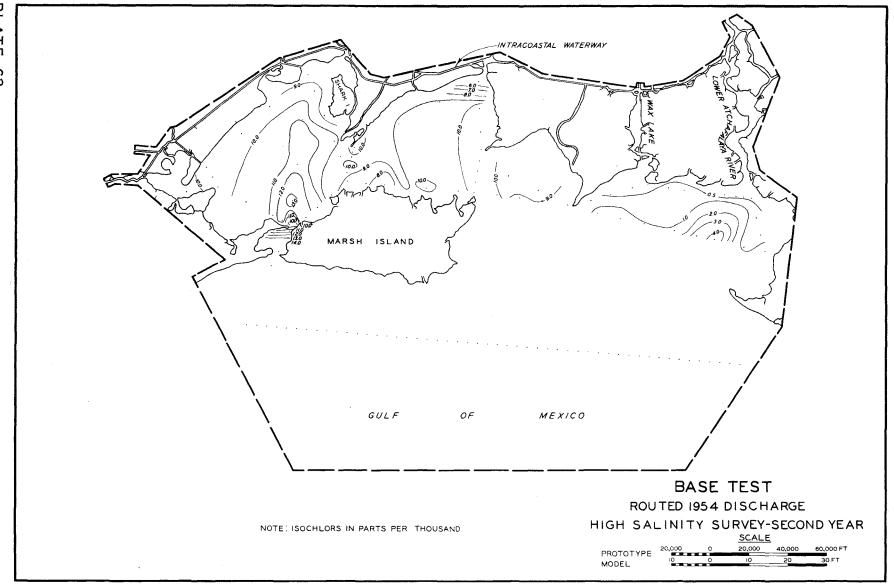


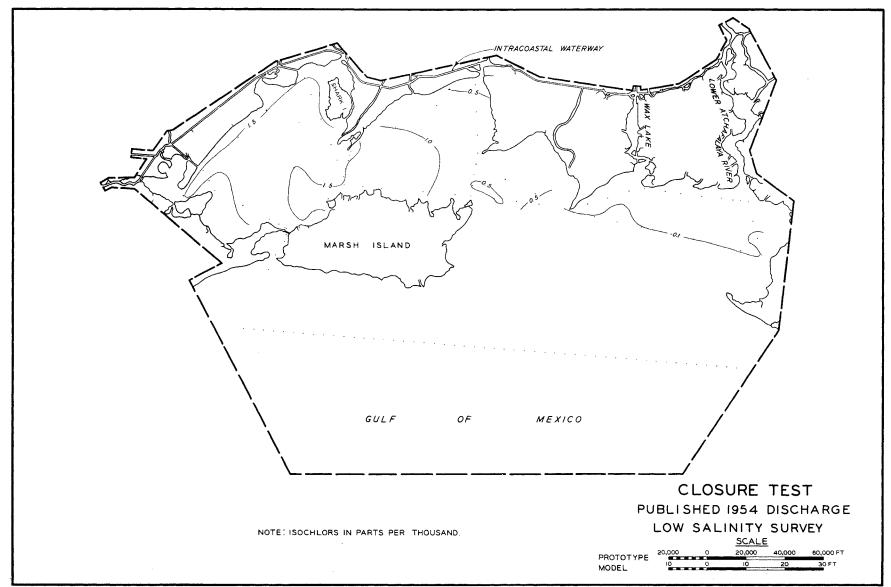


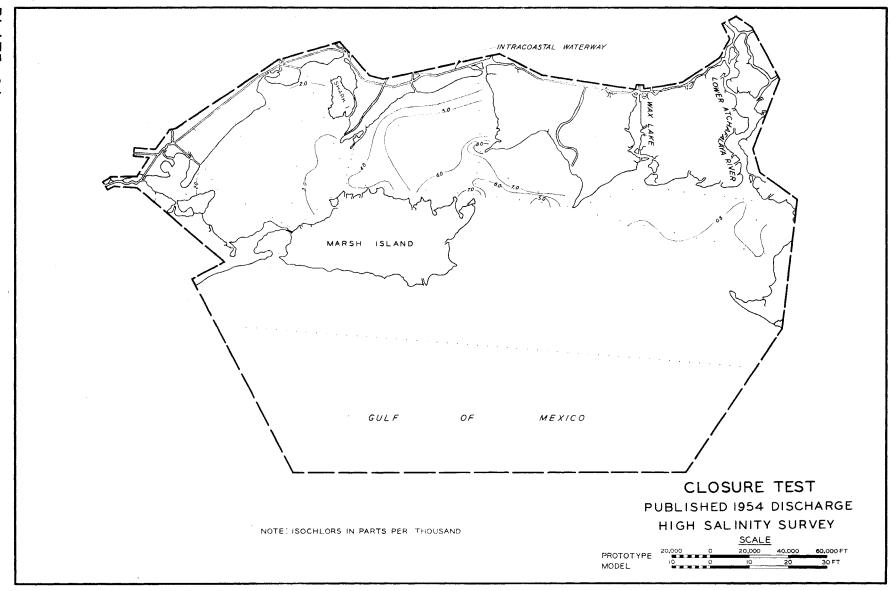


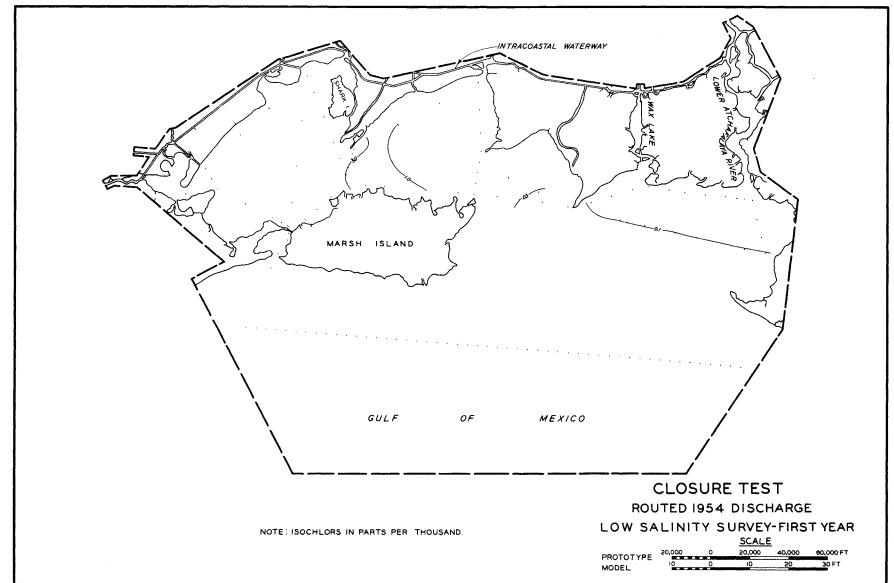


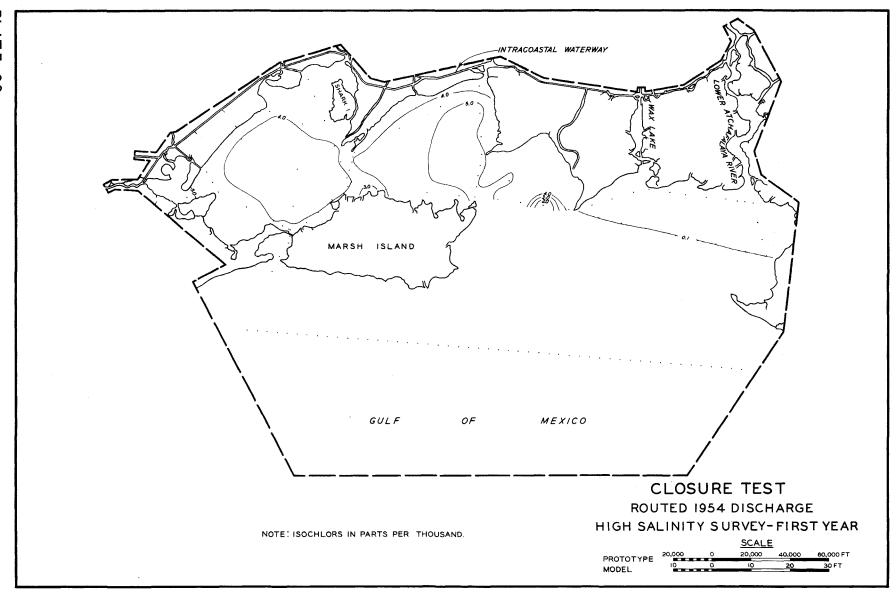


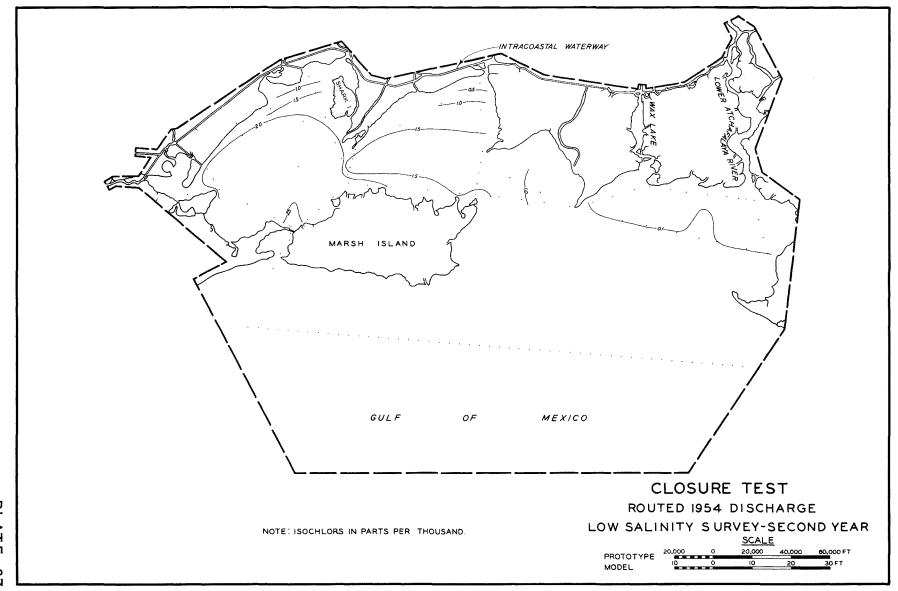


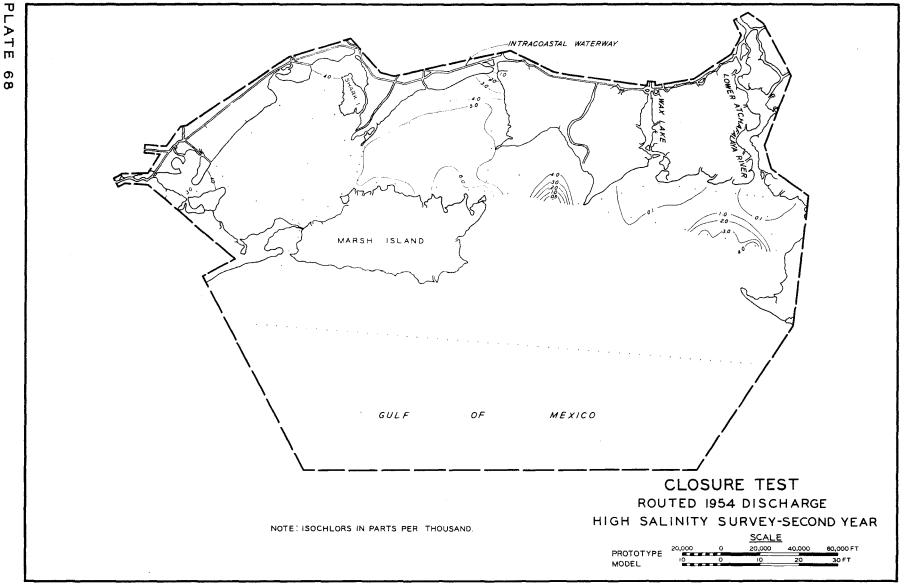


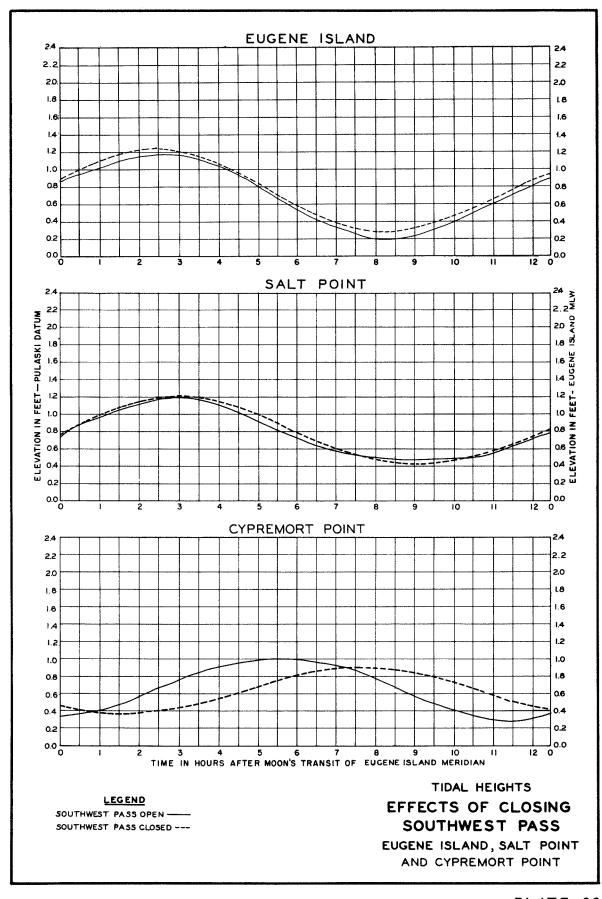


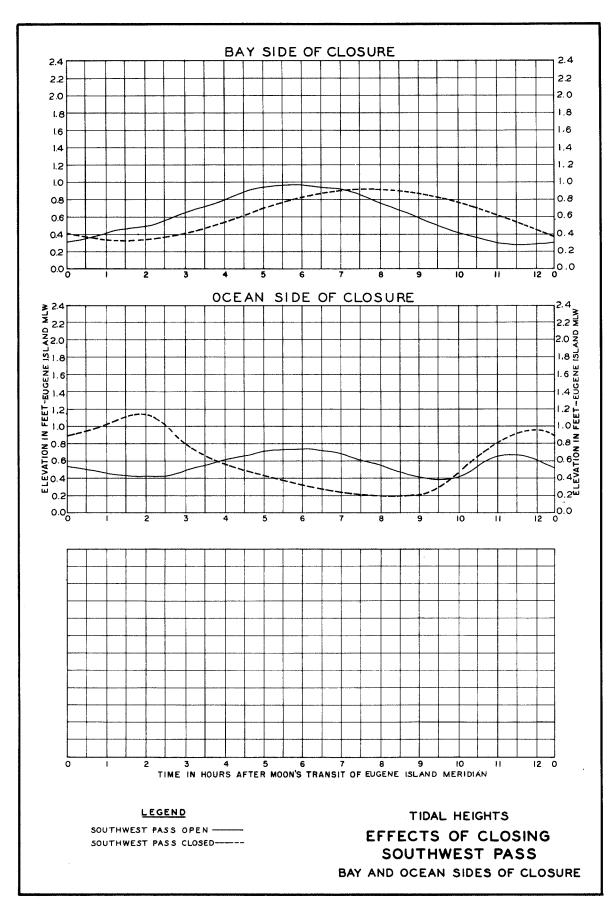


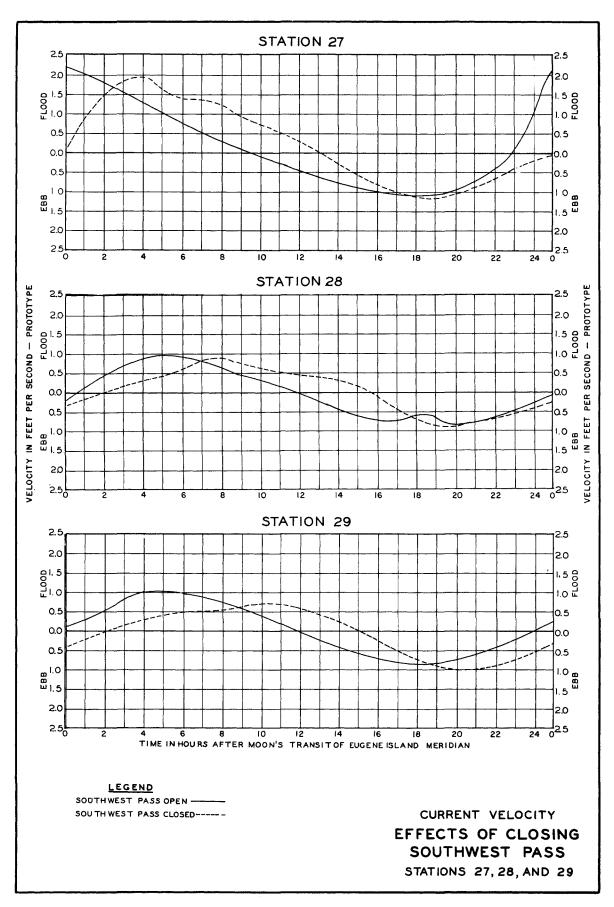


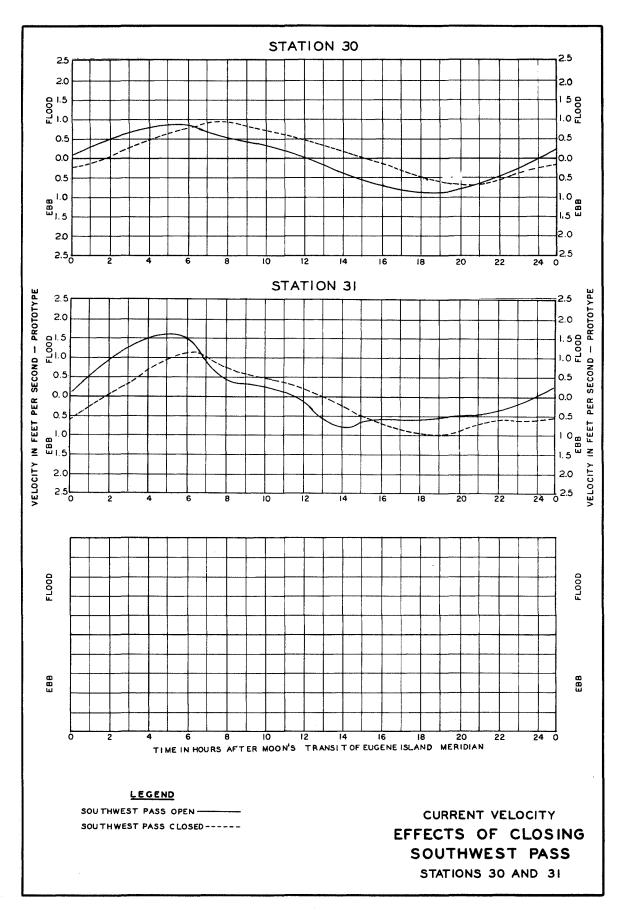


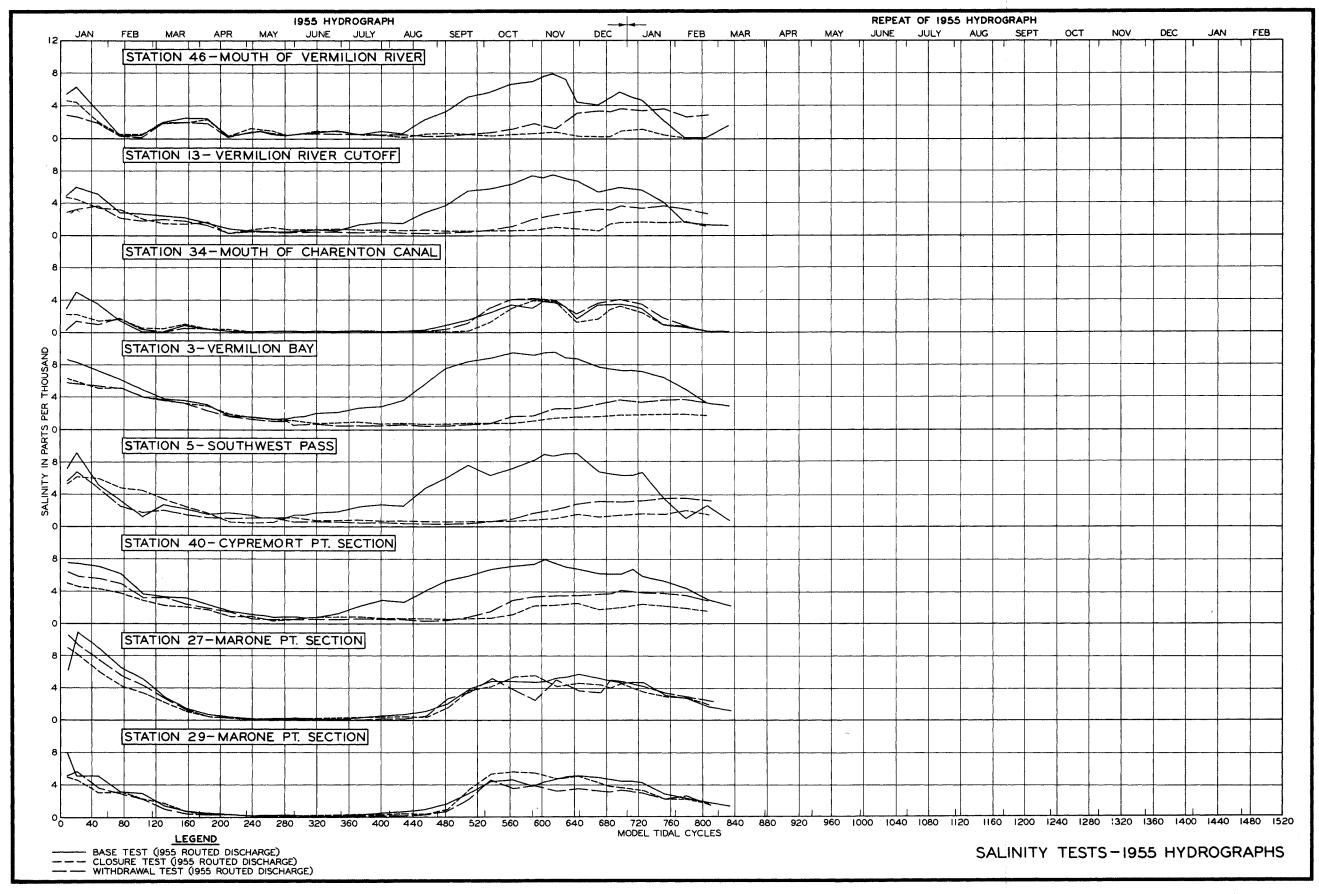












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